

Canterbury Olympic Ice Rink Redevelopment

Noise Impact Assessment Report

Prepared for: The Ice Skating Club of NSW Co-Operative Limited C/-Hunter Scott

Project No: SYD2599
Date: 2 August 2024
Revision: 04



Project: Canterbury Olympic Ice Rink Redevelopment

Location: 17A Phillips Ave,
Canterbury, NSW 2193

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Project No: SYD2599

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1. Introduction

ADP Consulting Pty Ltd has been engaged by *The Ice-Skating Club of NSW Co-Operative Limited* to provide acoustic engineering services for the proposed redevelopment of the Canterbury Olympic Ice Rink at 17A Phillips Ave, Canterbury NSW 2193.

The following are addressed:

- > Noise impacts to the proposed development and treatment recommendations to meet acoustic requirements.
- > Potential noise impacts from the operation of the proposed redevelopment and treatment recommendations to meet acoustic requirements for the amenity of the surrounding noise sensitive receivers.

The acoustic design criteria and treatment concepts in this report demonstrate the pathways by which these shall be addressed by ADP Consulting and the project team through further analysis, recommendations, and coordination as the design progresses.

1.1 Referenced Drawings, Codes and Standards

The following drawings, conditions, guidelines, standards, regulatory requirements, and other project-specific information have been referenced in preparing this report:

- > Architectural drawings (project number 2221) dated 31 May 2024 provided by Kennedy Associates Architects.
- > Canterbury Bankstown Council Development Control Plan (DCP) 2023.
- > AS 2670.2:1990 *Evaluation of Human Exposure to Whole-Body Vibration Part 2: Continuous and Shock-Induced Vibration in Buildings* (1 to 80 Hz) (AS 2670.2).
- > BS 6472–1992 – *Evaluation of Human Exposure to Whole-Body Vibration in Buildings* (1 to 80 Hz) (BS 6472).
- > AS/NZS 1668.1:2015 *The Use of Ventilation and Air Conditioning in Buildings Part 1: Fire and Smoke Control in Buildings* (AS/NZS 1668.1).
- > AS/NZS 2107:2016 *Acoustics – Recommended Design Sound Levels and Reverberation Times for Building Interiors* (AS/NZS 2107).
- > NSW Department of Environment and Conservation *Assessing Vibration: A Technical Guideline* dated February 2006 (AVTG).
- > NSW EPA *Noise Policy for Industry*, dated October 2017 (NPfI).
- > Transport & Infrastructure *State Environmental Planning Policy* 2021 (SEPP).
- > NSW EPA *Road Noise Policy*, dated March 2011 (RNP).

1.2 Project Summary

This report presents an analysis of the noise impacts associated with the proposed redevelopment of the Canterbury Olympic Ice Rink located at 17A Phillips Ave, Canterbury NSW 2193. The proposed redevelopment will include an expansion of the existing building to the north-west towards Tasker Park Playground as outlined in Figure 1 and Figure 2 below.

Consulting : Engineering

The current operational hours of the rink are between 5:30am and 11:30pm 7 days a week and activities at the rink include figure skating, ice hockey and public skating. There is no proposed change to the operation hours or activities in the building including no change to deliveries or waste removal in front of the building.

Figure 1 Ground floor with proposed expansion (in green) and existing spaces (in orange)

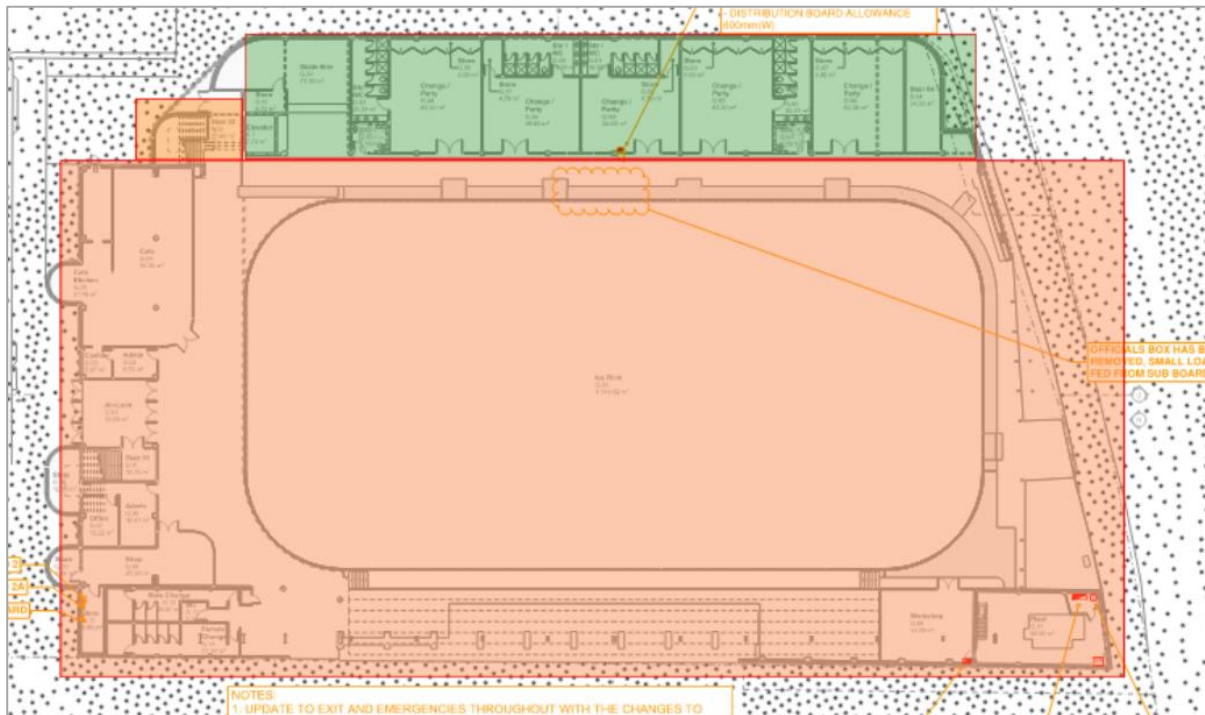
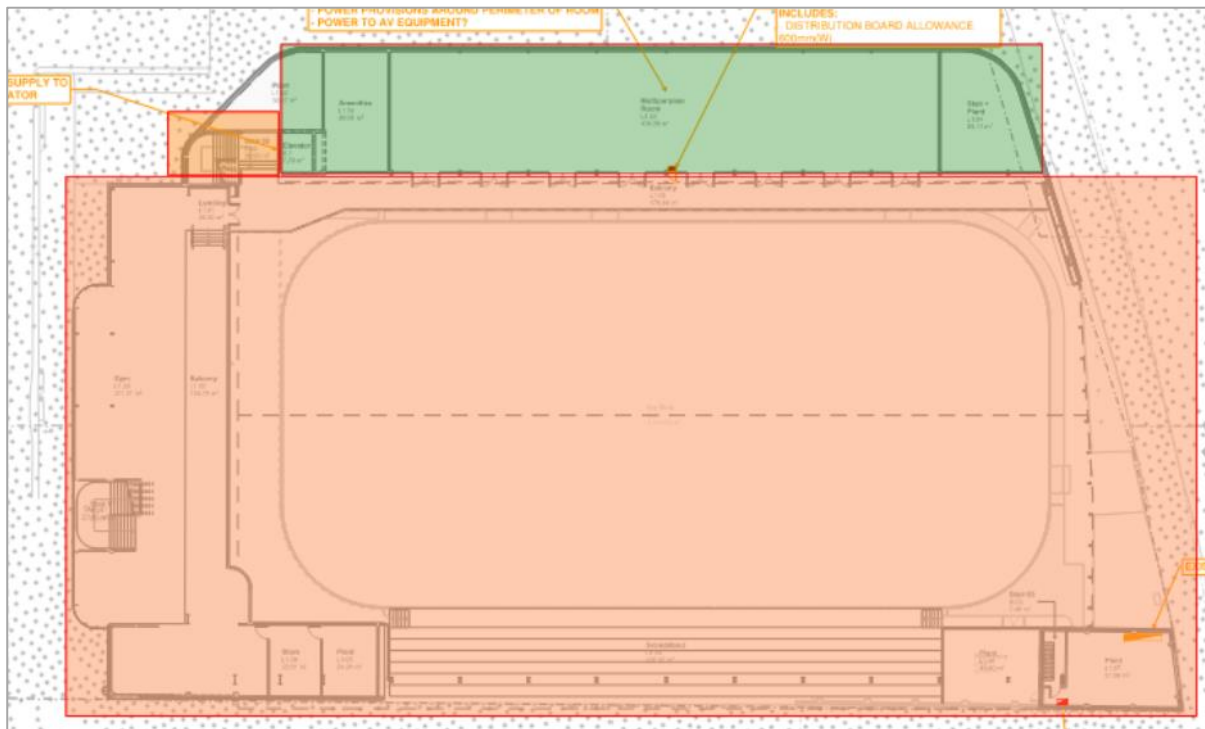


Figure 2 First floor with proposed expansion (in green) and existing spaces (in orange)



The proposed redevelopment includes new spaces to improve the amenities previously provided and are as follows:

- > Ground floor level:
 - Change rooms
 - Skate workshop and hire area
 - Storage space
- > First floor level:
 - Multipurpose room
 - Change rooms
 - Plant room

The existing building includes:

- > Ground floor level:
 - Entry area
 - Café with kitchen space
 - Shop
 - Cashier room
 - Offices
 - Admin spaces
 - Existing storage spaces
 - Storage space and workshop for ice machines
 - Plant rooms
 - Ca. 1.700m² ice rink
- > First floor level:
 - Grandstand
 - Warm-up area
 - Kitchen
 - Existing plant rooms
 - Storage spaces

The existing and proposed building includes thermally insulated panels limit noise emission from internal activities. Noise emission from internal activities is not expected to increase based on no change to the activities or number of patrons, only an improvement in amenities previously provided.

Additional services associated with the new spaces may introduce noise and are assessed.

1.3 Site Analysis

The development site is located at 17A Phillips Ave, Canterbury NSW 2193.

A site investigation was undertaken to identify noise sources that will potentially impact the project redevelopment, as well as the nearest noise sensitive receivers that will potentially be impacted by the proposed redevelopment.

The subject site is bounded by the following traffic and rail noise sources:

- > Wairoa Street directly to the west which carries low to medium volumes of traffic flow.
- > Phillips Avenue directly to the south which carries low to medium volumes of traffic flow.
- > T2 and T3 Rail Line directly to the north.

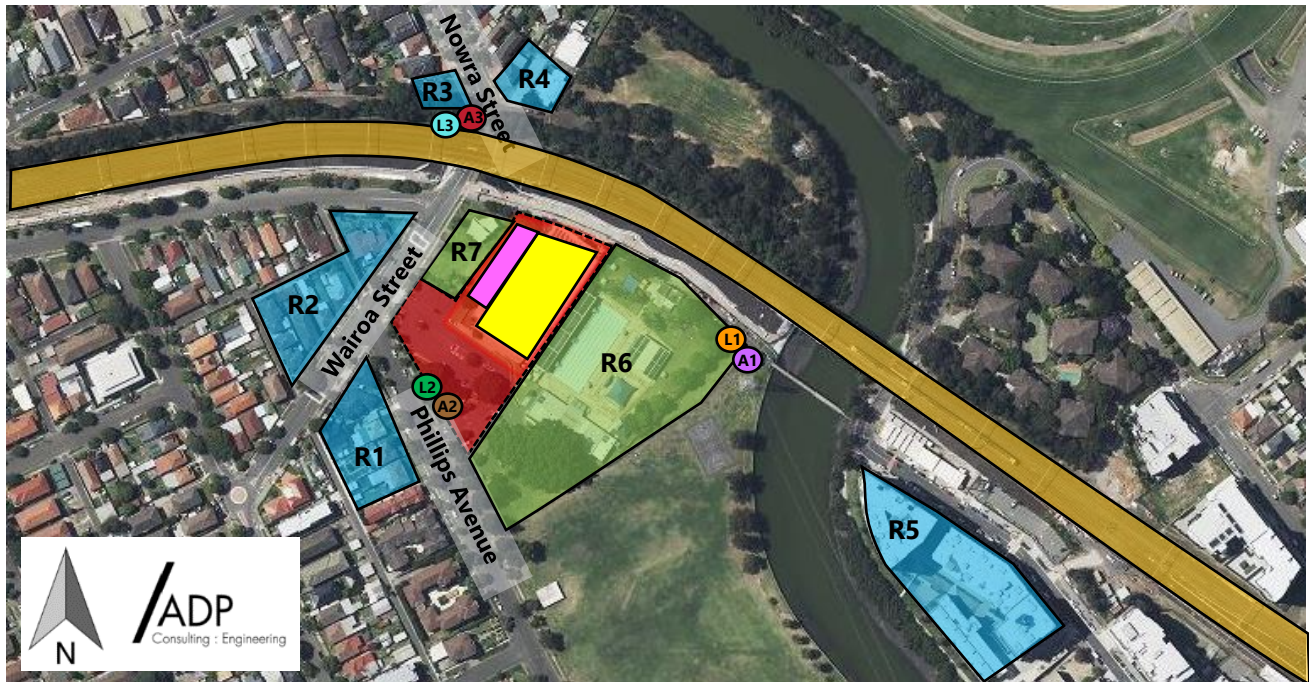
The following nearest most affected noise sensitive receivers were identified:

- > Residential receivers:
 - Receiver 1 (R1) – One to two-storey residential buildings located at 34 to 40 Phillips Avenue and 3-5 Wairoa Street, opposite of the project site to the south.

- Receiver 2 (R2) – One to two-storey residential buildings located at 8-12 Wairoa Street and 2 S Parade, opposite of the project site to the west.
- Receiver 3 (R3) – Two-storey residential building located at 4 Nowra Street to the north of the proposed redevelopment, behind the railway line.
- Receiver 4 (R4) – Two-storey residential buildings located at 1 Nowra Street and 4 E Parade to the north of the project site, behind the railway line.
- Receiver 5 (R5) – Ten-storey residential apartment building located at 15 Charles Street, east of the proposed redevelopment site.
- > Public Recreation receivers:
 - Receiver 6 (R6) – Canterbury Leisure and Aquatic Centre directly to the east of the project site.
 - Receiver 7 (R7) – Tasker Park Playground directly to the west of the project site.
- > The development itself that includes:
 - Plant and equipment requiring noise attenuation and vibration isolation to meet indoor noise level criteria in occupied areas and compliance with noise emission regulations.
 - An expected standard of amenity compliant with all applicable codes, regulatory requirements, client brief and/or other standards.

An aerial photograph including details of the proposed redevelopment is presented below in Figure 3.

Figure 3 Subject site and surrounding receivers zoning (Resourced from SIX Maps).



- Subject site
- Existing building
- Proposed Expansion
- Nearest residential noise sensitive receivers
- Nearest public recreation zone
- T2 and T3 Rail Line
- L1: Long-term noise monitoring location 1
- L2: Long-term noise monitoring location 2
- L3: Long-term noise monitoring location 3
- A1: Attended noise measurement (At logging location L1, next to T2 and T3 Rail Line)
- A2: Attended noise measurement (At logging location L2)
- A3: Attended noise measurement (3m away from kerb of Nowra Street, at logging location L3)

2. Existing Acoustic Environment

2.1 Instrumentation

The following instrumentation was used for noise measurement and analysis:

- > Bruel and Kjaer 2250 Integrating Sound Level Meter (S/N: 3011318).
- > Bruel and Kjaer type 1 microphone – comprising of:
 - ZC 0032 preamplifier (S/N: 25754).
 - 4189 capsule (S/N: 3087045).
- > Bruel and Kjaer Sound calibrator Type 4231 (S/N: 3018299).
- > Three (3) NSRT mk3 Sentry Noise Loggers.

Equipment is laboratory calibrated and certified within the last two years thus conforming to Australian Standards. Equipment was also field calibrated prior to and after noise surveys. Calibration drift was found to be less than 0.2dB during measurements, therefore no adjustments for instrument drift during the measurement period were warranted.

2.2 Long-term Noise Monitoring

Long-term noise monitoring was conducted between Monday 17th June and Monday 24th June 2024 at the following locations (also shown in Figure 3):

- > **Location L1:** At the eastern side boundary of the Leisure and Aquatic Centre, approximately 2m above ground level.
- > **Location L2:** At the southern site boundary towards residential receivers on Phillips Avenue, approximately 2m above ground level.
- > **Location L3:** North of the T2 & T3 Rail Line, at residential receiver R3, approximately 1.5m above ground level.

Measured background noise levels were corrected for meteorological conditions (wind above 5m/s and/or rain), as required by Section 3.4 of the EPA Noise Policy for Industry.

Background noise levels (L_{A90}) at locations L1, L2 and L3 are summarised in Table 1 below. Appendix B – Long-term Noise Monitoring Data presents detailed results of the unattended noise monitoring of logger locations L1, L2 and L3.

Table 1 Unattended noise measurements at Locations L1, L2 and L3, dB(A)

Noise Measurement	Daytime (7am-6pm)	Evening (6pm-10pm)	Night-time (10pm -7am)
Location L1			
Rating Background Level (RBL) – L _{A90}	46	44	38
Location L2			
Rating Background Level (RBL) – L _{A90}	45	44	39
Location L3			
Rating Background Level (RBL) – L _{A90}	41	40	34

2.3 Attended Noise Measurements

Attended noise measurements were conducted around the project site at 17A Phillips Ave, on Monday 17th June and Monday 24th June 2024 at the following locations:

- > **Location A1:** Attended 10-minute background noise measurement was undertaken at the eastern boundary of the Leisure and Aquatic Centre. The microphone was placed 1.5m above ground floor level.
- > **Location A2:** Attended 10-minute background noise measurement was undertaken at the southern site boundary towards residential receivers on Phillips Avenue. The microphone was placed 1.5m above ground floor level with 180 degrees view of Phillips Avenue.
- > **Location A3:** Attended 10-minute traffic noise measurement was undertaken at residential receiver R3, 3m away from the kerb of Nowra Street. The microphone was placed 1.5m above ground floor level with 180 degrees view of Nowra Street.

The noise measurements detailed above were used to qualify and quantify the long-term measured noise levels of the area. Table 2 presents the noise levels of the attended measurements at the locations shown in Figure 3.

Table 2 Attended noise measurements, dB(A).

Location	Start Time	Date	dB(A), L _{eq,t}	dB(A), L _{A90}
A1	12:45pm-13:00pm	17/06/2024	58	53
A2	15:05pm-15:10pm	24/06/2024	57	45
A3	14:55pm-15:05pm	24/06/2024	65	42

3. Noise Emission Criteria

Noise emissions from the operation of the proposed development to noise sensitive receivers shall be assessed for compliance criteria presented in this section.

The following sections outline the applicable policies, standards and guidelines that apply to environmental noise emission, and a summary of applicable environmental noise criteria is shown in Section 0.

3.1 Canterbury Bankstown Council Development Control Plan (DCP) 2023

The planning and design guidelines for the proposed development are presented in the Canterbury Bankstown Council Development Control Plan 2023. The DCP does not specify criteria regarding noise emission criteria for commercial developments and therefore is not considered further for this assessment.

3.2 NSW Noise Policy for Industry (NPfI)

The NPfI requires compliance with specific *project noise trigger levels*, which are determined from the lower (that is, the more stringent) value of the project *intrusiveness noise level* and project *amenity noise level*. The NPfI also includes the application of modifying factors for undesirable noise characteristics such as tonality or impulsiveness, up to a maximum of 10dB.

3.2.1 Noise Intrusiveness

The NPfI states that the intrusiveness of an industrial noise source may generally be considered acceptable if the equivalent continuous (energy-average) A-weighted level of noise from the source (represented by the L_{Aeq} descriptor), measured over a 15-minute period, does not exceed the background noise level (L_{A90}) measured in the absence of the source by more than 5dB.

The relevant noise intrusiveness levels applicable to this project are shown in Table 3, Table 4 and Table 5.

Table 3 Noise intrusiveness noise levels Residential receivers R1 and R2

Time of operation	Background noise Level dB(A) L_{90}	Intrusiveness criteria, $L_{Aeq,15min}$ (Background + 5dB)
Day (7am to 6pm)	45	50
Evening (6pm to 10pm)	44	49
Night (10pm to 6am)	39	44

Table 4 Noise intrusiveness noise levels Residential receivers R3 and R4

Time of operation	Background noise Level dB(A)L ₉₀	Intrusiveness criteria, L _{Aeq,15min} (Background+5dB)
Day (7am to 6pm)	41	46
Evening (6pm to 10pm)	40	45
Night (10pm to 6am)	34	39

Table 5 Noise intrusiveness noise levels Residential receiver R5

Time of operation	Background noise Level dB(A)L ₉₀	Intrusiveness criteria, L _{Aeq,15min} (Background+5dB)
Day (7am to 6pm)	46	51
Evening (6pm to 10pm)	44	49
Night (10pm to 6am)	38	43

3.2.2 Amenity Noise Levels

The NPfI describes methodology to limit gradual increases in noise levels from the introduction of new noise sources in an area.

The *recommended amenity noise levels* represent the objective for total industrial noise at a receiver location, whereas the *project amenity noise level* represents the objective for noise from this project. The *project amenity noise level* for industrial developments = *recommended amenity noise level* (Table 2.2) minus 5 dB(A). 3 dB is then added to convert from an L_{Aeq,T} period to L_{Aeq, 15min}.

NPfI Table 2.2 specifies maximum amenity noise levels for different types of receivers. The relevant amenity noise levels applicable to this project are shown in Table 6.

Table 6 Recommended amenity noise levels and project amenity noise levels

Receiver	Noise Amenity Area	Time of day	Recommended amenity noise levels, $L_{Aeq, period}$	Project amenity noise levels, $L_{Aeq, 15min}$
Residential	Suburban	Day	55	53
		Evening	45	43
		Night	40	38
Public recreation area	All	When in use	50	-

Note 1: Table 2.1 of the NPfI has four categories of residential areas: rural, suburban, urban and urban/industrial. The nearest noise sensitive residential receivers around the proposed development are considered as "suburban".

3.2.3 Modifying Factors

Undesirable characteristics such as tonality, low frequency, impulsiveness and intermittency, adjustments (as per Fact Sheet C of the NPfI) shall be assessed. These modifying factors include a 5dB penalty for each undesirable characteristic. A maximum penalty of 10dB for 2 or more undesirable characteristics applies.

3.2.4 Sleep Disturbance

NPfI establishes sleep disturbance criteria for residential noise sensitive receivers for noise events during the night period. The sleep disturbance criteria are summarised below:

- $L_{Aeq,15min}$ 40 dB(A) or prevailing RBL plus 5dB, whichever is greater, and/or
- L_{AFmax} 52 dB(A) or prevailing RBL plus 15dB, whichever is greater.

Table 7 Sleep disturbance criteria

Receivers	Night-time level dB(A) L_{90}	Sleep disturbance level
Residential Receivers R1 and R2	39	$L_{Aeq,15min}$ dB(A) 44
		L_{AFmax} dB(A) 54
Residential Receivers R3 and R4	34	$L_{Aeq,15min}$ dB(A) 40
		L_{AFmax} dB(A) 52
Residential Receiver R5	38	$L_{Aeq,15min}$ dB(A) 43
		L_{AFmax} dB(A) 53

3.3 Summary of Noise Emission Criteria

A summary of noise emission criteria that applies at residential receivers from the use of the proposed development is presented in the following tables.

The 'project trigger levels' are the most stringent noise criteria that apply in each instance, i.e., they are expected to be the 'driving' criteria.

Table 8 Noise emission criteria – Residential receivers R1 and R2

Time of operation	Intrusiveness criteria, $L_{Aeq,15min}$ (Background + 5dB)	Recommended amenity noise levels, $L_{Aeq, period}$	Project amenity noise levels, $L_{Aeq, 15min}$	Project trigger levels, $L_{Aeq, 15min}$
Day (7am to 6pm)	50	55	53	50
Evening (6pm to 10pm)	49	45	43	43
Night (10pm to 6am)	44	40	38	38 Sleep Disturbance $44L_{Aeq (15min)} /$ $54L_{Max}$

Table 9 Noise emission criteria – Residential receivers R3 and R4

Time of operation	Intrusiveness criteria, $L_{Aeq,15min}$ (Background + 5dB)	Recommended amenity noise levels, $L_{Aeq, period}$	Project amenity noise levels, $L_{Aeq, 15min}$	Project trigger levels, $L_{Aeq, 15min}$
Day (7am to 6pm)	46	55	53	46
Evening (6pm to 10pm)	45	45	43	43
Night (10pm to 6am)	39	40	38	38 Sleep Disturbance $40L_{Aeq (15min)} /$ $52L_{Max}$

Table 10 Noise emission criteria – Residential receiver R5

Time of operation	Intrusiveness criteria, $L_{Aeq, 15min}$ (Background + 5dB)	Recommended amenity noise levels, $L_{Aeq, period}$	Project amenity noise levels, $L_{Aeq, 15min}$	Project trigger levels, $L_{Aeq, 15min}$
Day (7am to 6pm)	51	55	53	51
Evening (6pm to 10pm)	49	45	43	43
Night (10pm to 6am)	43	40	38	38 Sleep Disturbance $40L_{Aeq, (15min)} / 52L_{Max}$

Table 11 Noise emission criteria – Public recreation receivers R6 and R7

Receiver	Time of operation	Site specific noise limits	
		Recommended amenity, $L_{Aeq, Period}$	Project trigger levels, $L_{Aeq, 15min}$
R6 / R7	When in use	50	-

4. Internal Noise Requirements

External noise sources that can potentially affect the proposed development include road traffic passing the site. Noise intrusions to the proposed development from this noise source will be assessed in accordance with the criteria presented in this section.

4.1 Canterbury Bankstown Council Development Control Plan (DCP) 2023

The planning and design guidelines for the proposed development are presented in the Canterbury Bankstown Council Development Control Plan 2023. The DCP does not specify criteria regarding noise intrusion to commercial developments and therefore is not considered further for this assessment.

4.2 State Environmental Planning Policy (Transport and Infrastructure) 2021

Clauses 2.119 and 2.120 of the State Environmental Planning Policy (Transport and Infrastructure) 2021 (SEPP), specifies indoor noise level requirements for development in frontage to classified road and land in or adjacent to the road corridor for a freeway, a tollway or a transitway or any other road with annual average daily traffic volume of more than 20,000 vehicles (based on the traffic volume data published on the website of TfNSW).

The nearest classified road to the proposed development is approximately 450m to the south-east (A34). Therefore, the SEPP criteria are not applicable to this project.

4.3 Australian/ New Zealand Standard AS/NZS 2107:2016

The internal noise criteria for the proposed expansion of the facility will be based on AS/NZS 2107:2016 Acoustics – Recommended Design Sound Levels for Building Interiors (AS/NZS 2107) internal design levels. Recommended indoor noise levels for the proposed redevelopment are summarised in Table 12 below.

Table 12 Internal design sound pressure levels for offices within the development

Type of occupancy (Commercial / sports buildings)	Time period	Design SPL, L_{Aeq} , dB(A)
Change rooms	When in use	45 to 55
Corridors and lobbies	When in use	45 to 50
Toilets / showers	When in use	45 to 55
Multipurpose room	When in use	40 to 45
Skate Hire / Skate Workshop	When in use	< 50
Storage	-	-
Plant rooms	-	-

5. Environmental Noise Emission Assessment

Noise emissions from the proposed redevelopment will need to be assessed to ensure compliance with the noise emission criteria as presented in Section 0.

5.1 Noise Assessment of Proposed Plant

The proposed plant changes include:

- > An external air handling unit located at on the COIR north east boundary
- > 2 internal air handling units located in enclosed plantrooms and ducted to external louvres
- > Fan Coil Unit outside air louvres
- > Exhaust fan louvres

An assessment of the introduced noise sources is as follows:

Based on typical AHU noise data, the noise criteria provided in Section 3 of this report is predicted to be met based on:

- > The proposed plant and equipment by ADP mechanical services with consideration to noise output.
- > Selection of low noise fans, allowance for smooth airflow conditions in ductwork, and lined duct work while minimising regenerated noise at bends, take-offs and transitions.

5.2 Vehicle Noise Assessment on Carpark

The proposed development is not expected to significantly increase patron numbers or existing car park operation; therefore, a new assessment is not required.

5.3 Patron Noise Assessment

The proposed development is not expected to significantly increase patron numbers or existing café operation; therefore, a new assessment is not required.

6. Noise Intrusion Assessment

The recommended building envelope acoustic treatments to control external noise are presented below, based on achieving the internal noise criteria presented in Section 4. The main source of external noise that will affect the proposed expansion of the existing building is road traffic along Wairoa Street as well as rail noise of T2 and T3 rail lines.

Treatments were determined based on the noise levels recorded at the site and presented in Section 2, and internal noise criteria outlined in Section 4. Calculations were undertaken considering the orientation of windows, barrier effects (where applicable), the total area of glazing, facade transmission loss and room sound absorption characteristics.

6.1 Glazing

Based on measured ambient sound pressure levels and the internal noise level criteria will be satisfied with a minimum glazing thickness of 6mm float glass. Thicker glazing, or double-glazed units may be required for thermal, structural or safety purposes. Where thicker glazing is required, this will also be acoustically acceptable.

Any openable windows and external doors are required to be fitted with polyurethane foam seals (Q-Lon or similar). Mohair seals are not acceptable.

6.2 External Walls

External masonry walls will not require any additional acoustic treatments. If penetrations are required to the external skin of the external walls, they shall be sealed with an acoustic-grade sealant.

6.3 External Doors/ Entry Doors

External solid core doors will be sufficient for acoustic purposes. External glass doors should comply with the minimum glazing performance requirements presented in Section 6.1.

Door seals are recommended (Q-lon seals by Schlegel or similar – mohair seals should be avoided).

6.4 Roof Construction

Roofs that feature a concrete slab construction will not require any additional acoustic treatment. If penetrations are required, they shall be sealed with an acoustic-grade sealant.

7. Conclusion

ADP Consulting has completed an acoustic assessment for the proposed redevelopment and expansion of the Canterbury Olympic Ice Rink at 17A Phillips Ave, Canterbury NSW 2193.

Noise emission criteria were setup in Section 3 based on:

- > Long-term noise monitoring results.
- > NSW Environmental Protection Authority (EPA) Noise Policy for Industry (NPfI) 2017.

Provided the recommended treatments in this report are adopted, the proposal will comply with the presented internal noise criteria in Section 3:

- > NSW Environmental Protection Authority (EPA) Noise Policy for Industry (NPfI) 2017.

A noise emission assessment has been undertaken and concludes that the mechanical plans and plant selections comply with the external noise criteria.

Appendix A

Glossary of Acoustic Terms

Air-borne sound

The sound emitted directly from a source into the surrounding air, such as speech, television or music.

Ambient sound

Of an environment: the all-encompassing sound associated with that environment, being a composite of sounds from many sources, near and far. This is normally taken to be the L_{Aeq} value.

Background noise level

The average of the lowest levels of the noise levels measured in an affected area in the absence of noise from occupants and from unwanted external ambient noise sources. Usually the L_{A90} value represents the background noise level.

dB(A)

Unit of acoustic measurement weighted to approximate the sensitivity of human hearing to sound frequency.

Decibel scale

The decibel scale is logarithmic in order to produce a better representation of the response of the human ear. Therefore, a 3 dB increase in the sound pressure level corresponds to a doubling in the sound energy. It is generally accepted that a 10 dB increase in the sound pressure level corresponds to a perceived doubling in loudness.

Examples of decibel levels of common sounds are as follows:

- > 0 dB(A) Threshold of human hearing
- > 30 dB(A) A quiet country park
- > 40 dB(A) Whisper in a library
- > 50 dB(A) Open office space
- > 70 dB(A) Inside a car on a freeway
- > 80 dB(A) Outboard motor
- > 90 dB(A) Heavy truck pass-by
- > 100 dB(A) Jackhammer / Subway train
- > 110 dB(A) Rock Concert
- > 115 dB(A) Limit of sound permitted in industry
- > 120 dB(A) 747 take off at 250 metres

Frequency

The repetition rate of the cycle measured in Hertz (Hz). The frequency corresponds to the pitch of the sound. A high frequency corresponds to a high-pitched sound and a low frequency to a low-pitched sound.

L_{90} , L_{10} , etc

A statistical measurement giving the sound pressure level which is exceeded for the given percentile of a measurement period (i.e. L_{90} is the level which is exceeded for 90 percent of a measurement period). L_{90} is commonly referred to as a basis for measuring the background sound level.

$L_{Aeq,T}$

The equivalent continuous A-weighted sound pressure level. The value of the A-weighted sound pressure level of a continuous steady sound that, within a measurement time interval T, has the same A-weighted sound energy as the actual time-varying sound.

L_{Amax}

The maximum sound pressure level measured over the measurement period.

L_{Amin}

The minimum sound pressure level measured over the measurement period.

Day

Referred to as the period between 7am and 6pm for Monday to Saturday and 8am to 6pm for Sundays and Public Holidays.

Evening

Referred to as the period between 6pm and 10pm for Monday to Sunday and Public Holidays.

Night

Referred to as the period between 10pm and 7am for Monday to Saturday and 10pm to 8am for Sundays and Public Holidays.

Assessment background level (ABL)

The overall background noise level on each day, evening and night periods for each day of the noise monitoring.

Rating background level (RBL)

The overall background level on each day, evening and night periods for the entire length of noise monitoring.

Reverberation

The persistence, after emission by the source has stopped, of a sound field in an enclosure.

Sound isolation

A reference to the degree of acoustical separation between two spaces. Sound isolation may refer to sound transmission loss of a partition or to noise reduction from any unwanted noise source. The term 'sound isolation' does not specify any grade or performance quality and requires the units to be specified for any contractual condition.

Sound pressure level, L_p, dB of a sound

A measurement obtained directly obtained using a microphone and sound level meter. Sound pressure level varies with distance from a source and with changes to the measuring environment. Sound pressure level equals 20 times the logarithm to the base 10 of the ratio of the R.M.S. sound pressure to the reference sound pressure of 20 micro-Pascals.

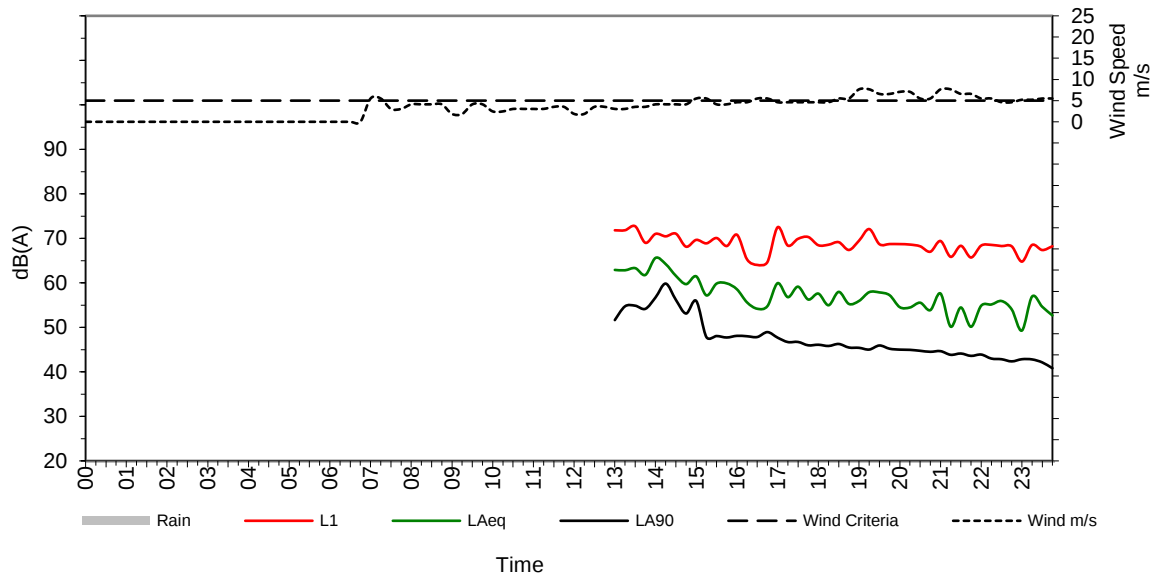
Appendix B

Long-term Noise Monitoring Data

Sentry 8 - Location L1

Monday 17 June 2024

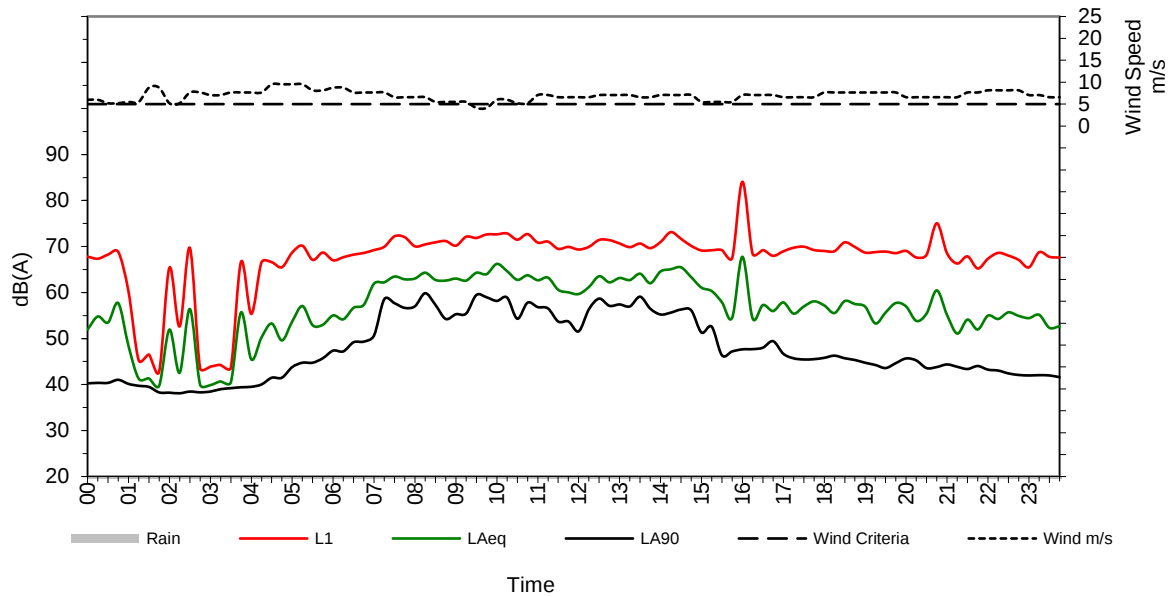
Noise Logger



Sentry 8 - Location L1

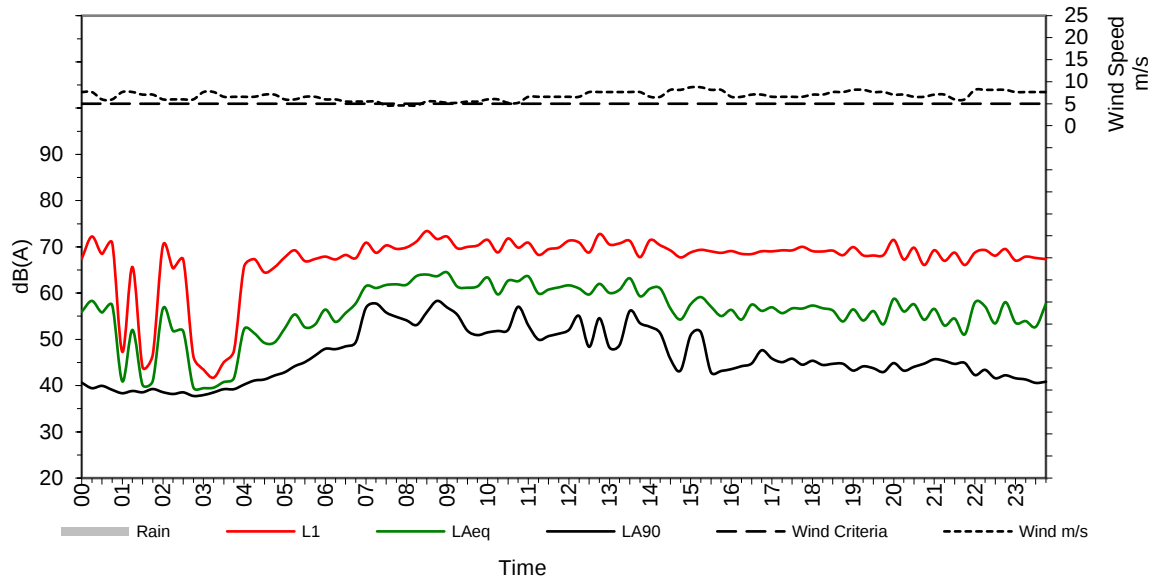
Tuesday 18 June 2024

Noise Logger



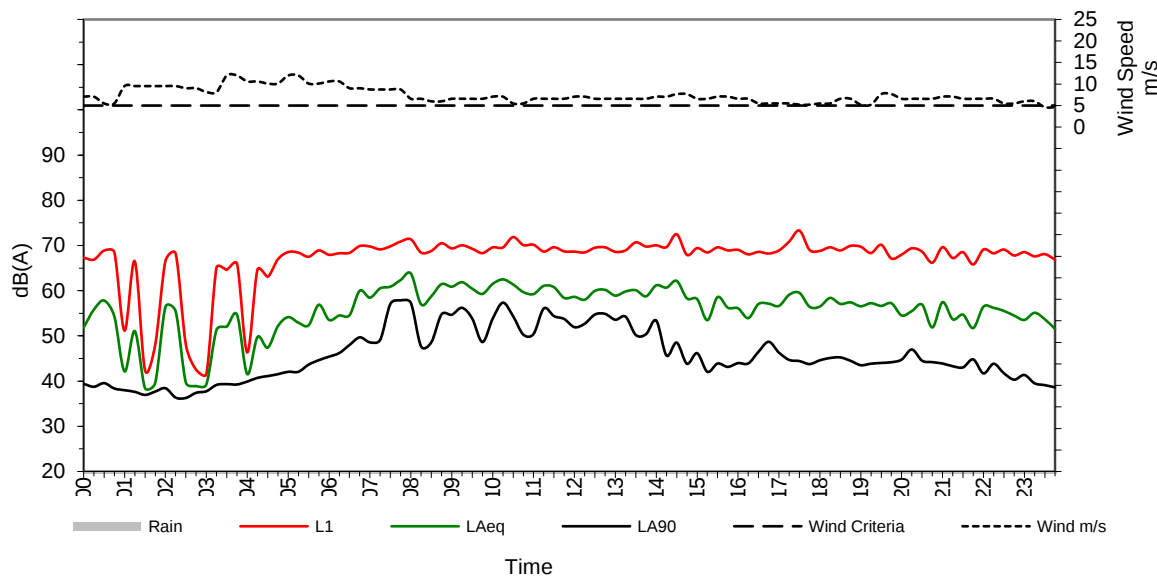
Sentry 8 - Location L1
Noise Logger

Wednesday 19 June 2024



Sentry 8 - Location L1
Noise Logger

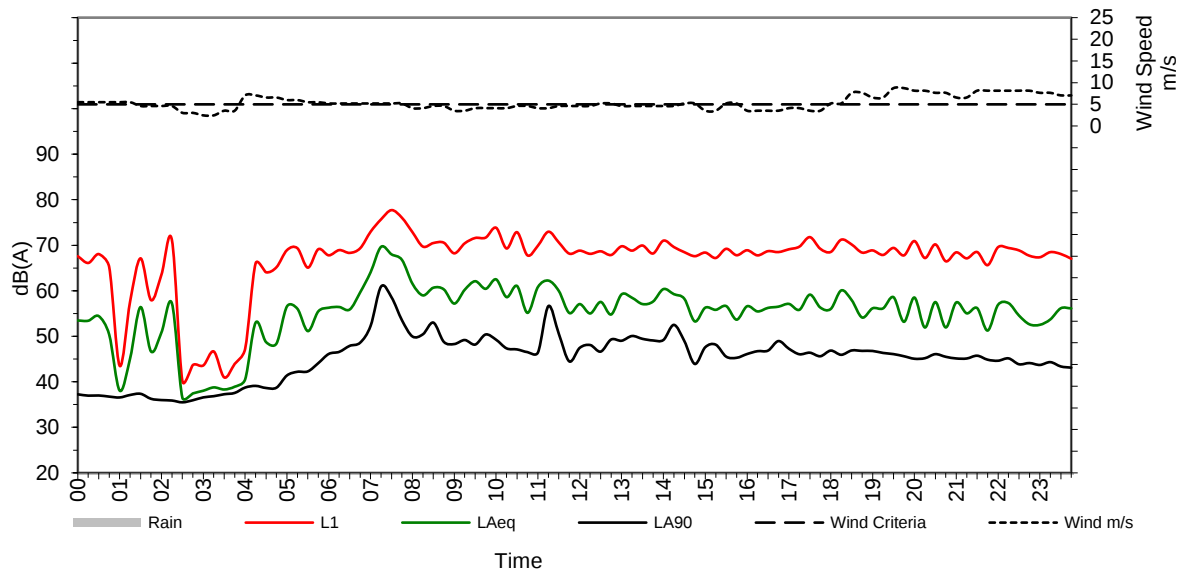
Thursday 20 June 2024



Sentry 8 - Location L1

Friday 21 June 2024

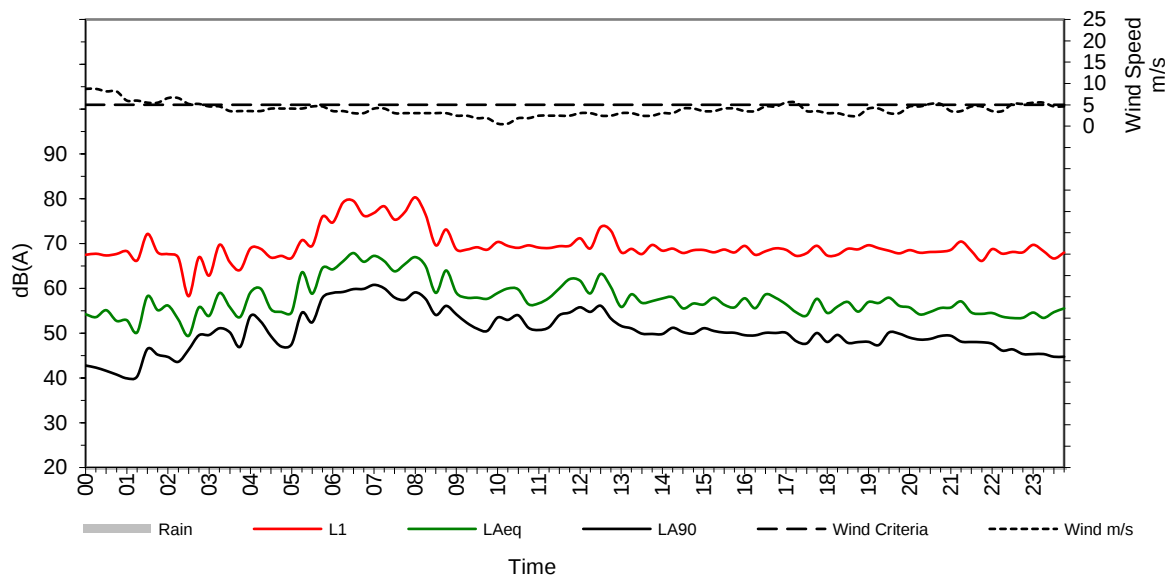
Noise Logger



Sentry 8 - Location L1

Saturday 22 June 2024

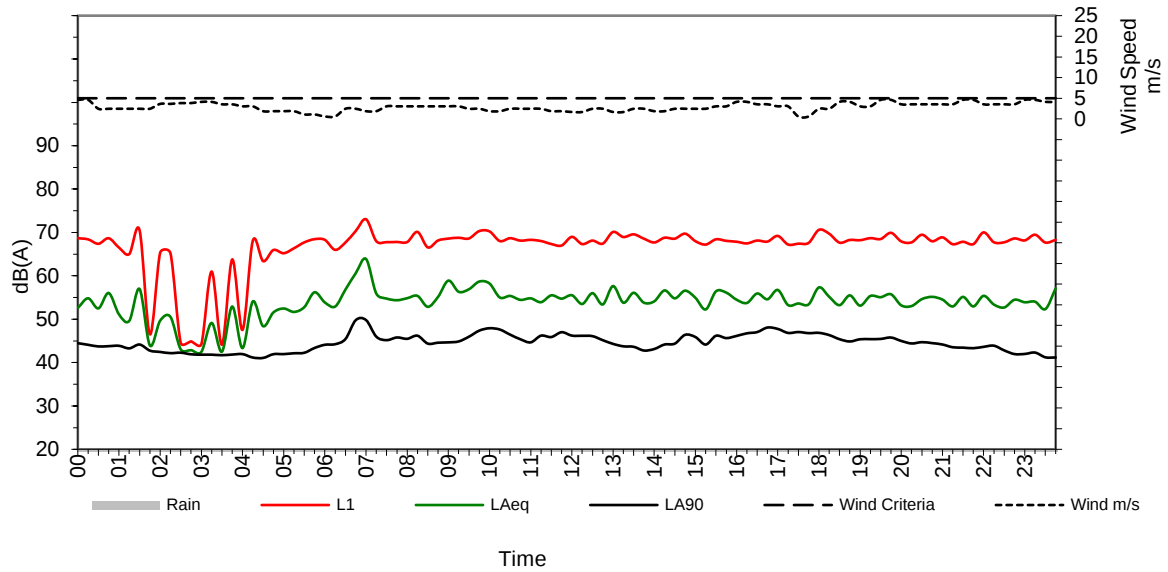
Noise Logger



Sentry 8 - Location L1

Sunday 23 June 2024

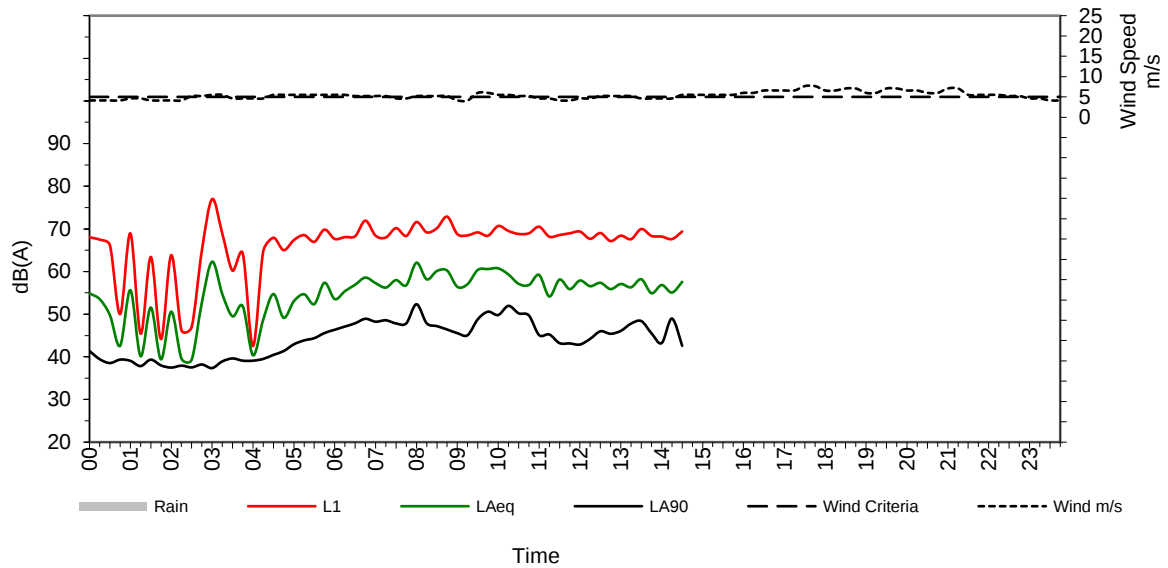
Noise Logger



Sentry 8 - Location L1

Monday 24 June 2024

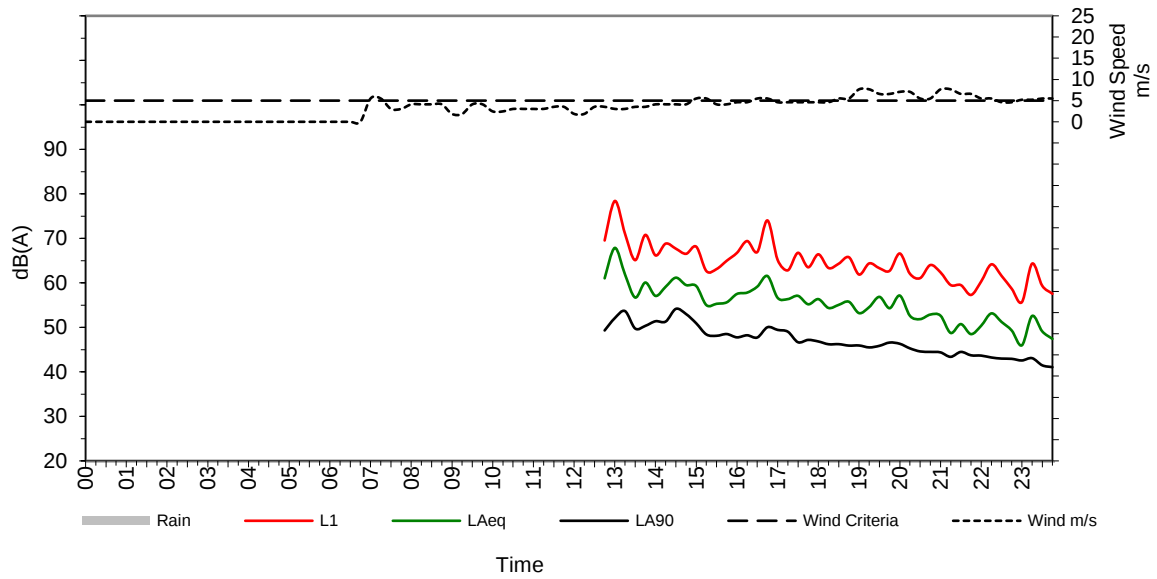
Noise Logger



Sentry 1 - Location L2

Monday 17 June 2024

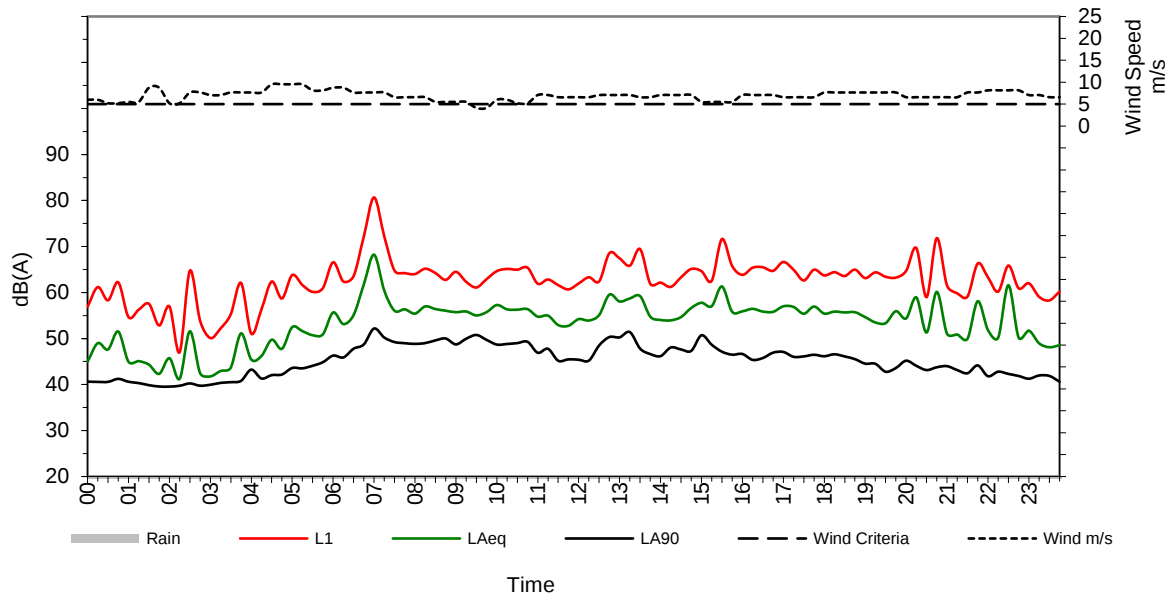
Noise Logger



Sentry 1 - Location L2

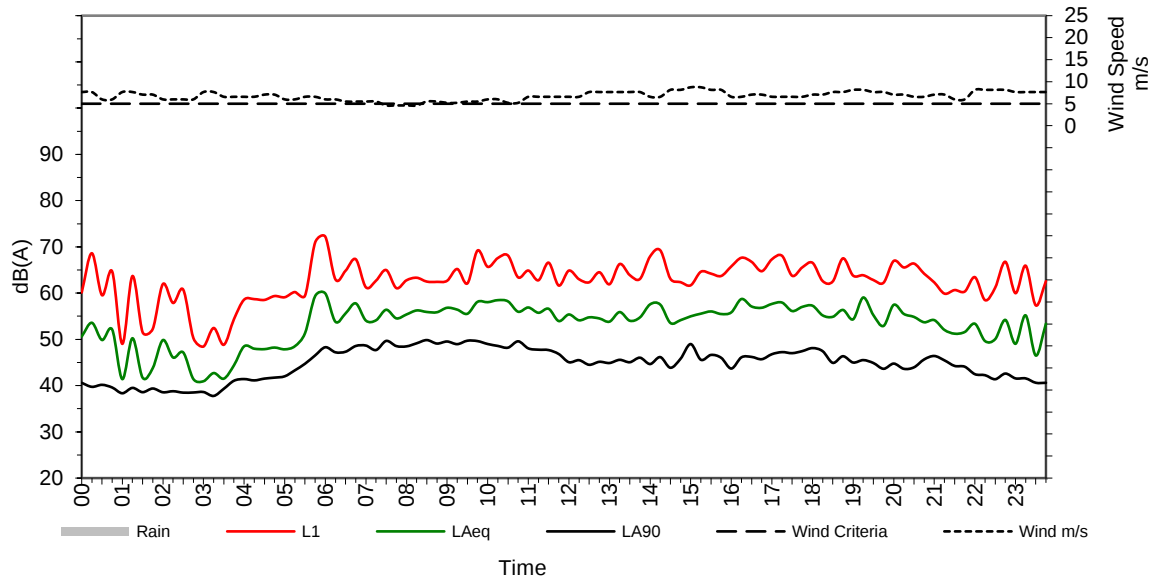
Tuesday 18 June 2024

Noise Logger



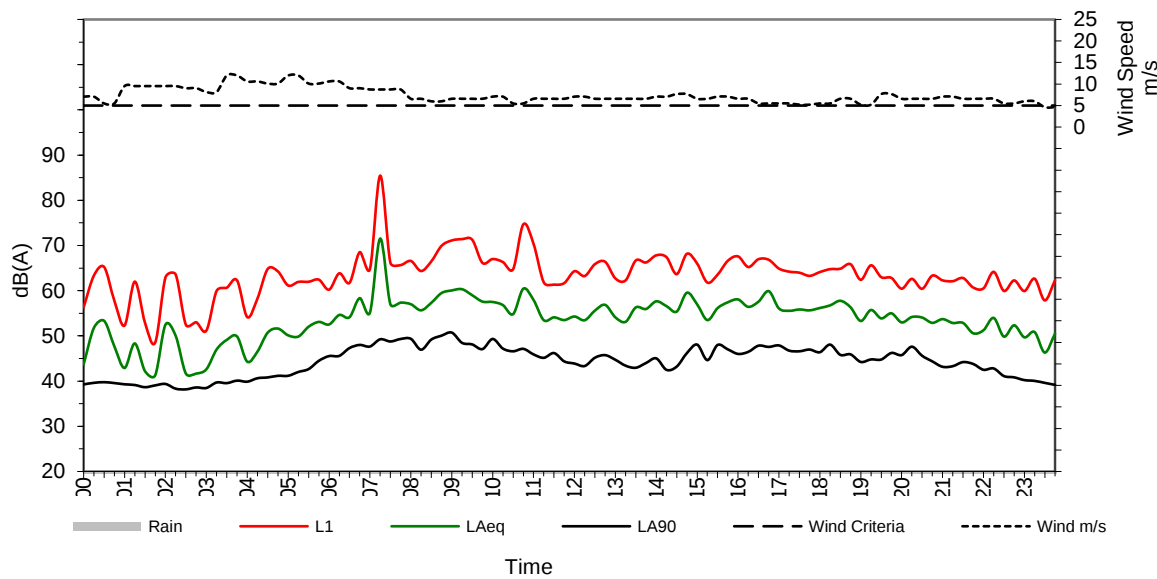
Sentry 1 - Location L2
Noise Logger

Wednesday 19 June 2024



Sentry 1 - Location L2
Noise Logger

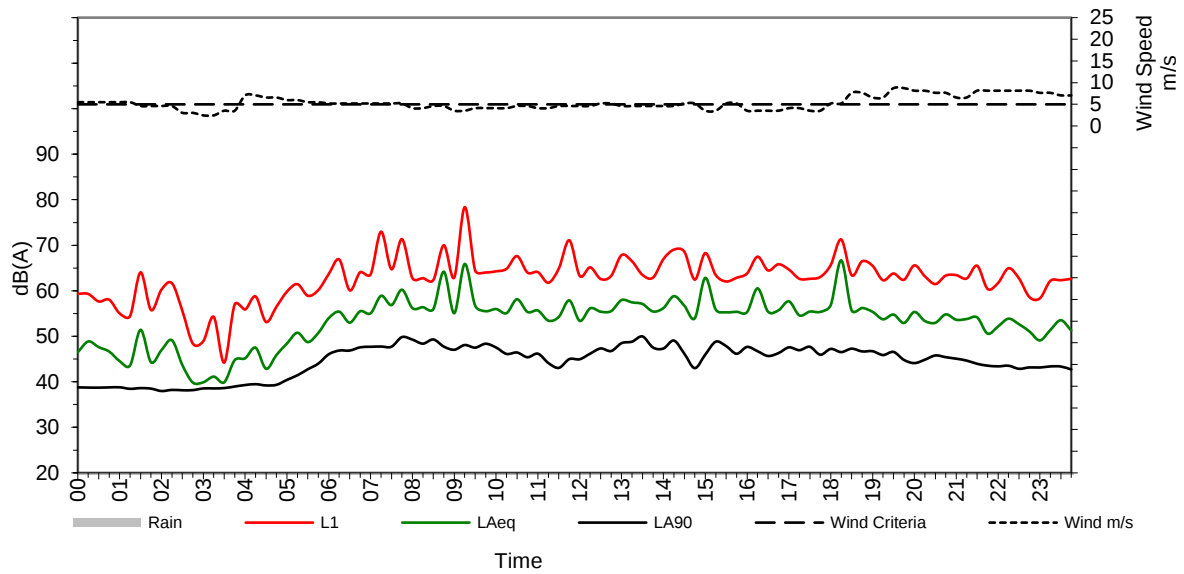
Thursday 20 June 2024



Sentry 1 - Location L2

Friday 21 June 2024

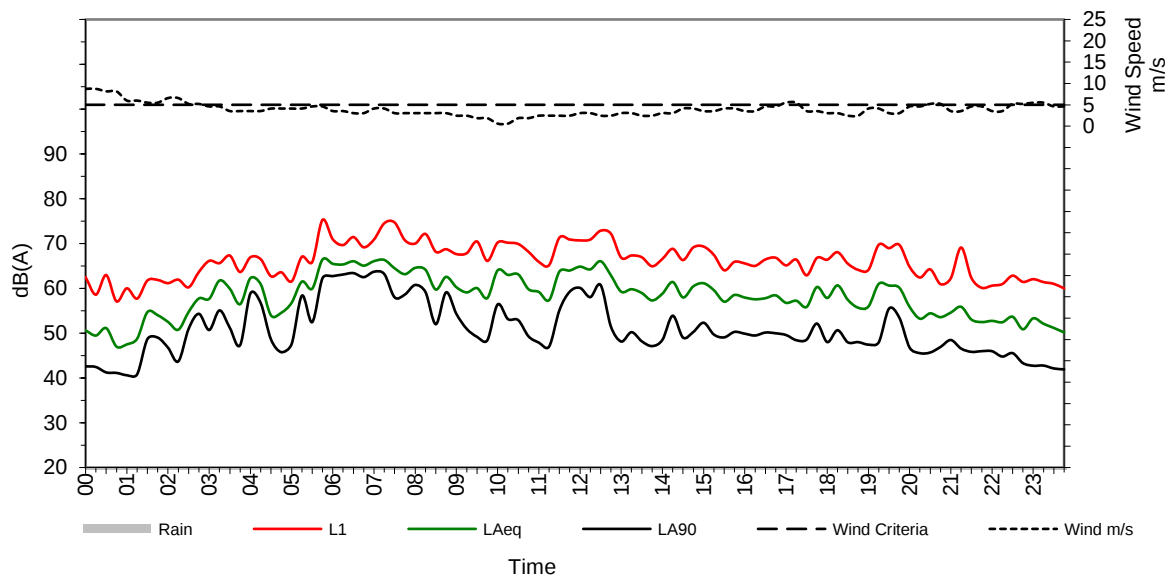
Noise Logger



Sentry 1 - Location L2

Saturday 22 June 2024

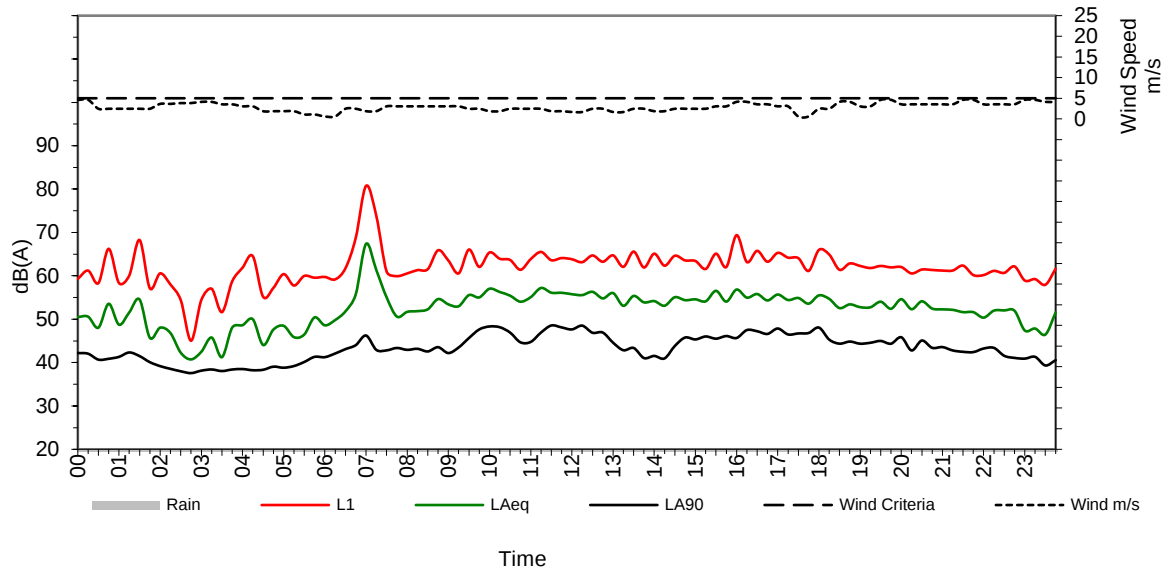
Noise Logger



Sentry 1 - Location L2

Sunday 23 June 2024

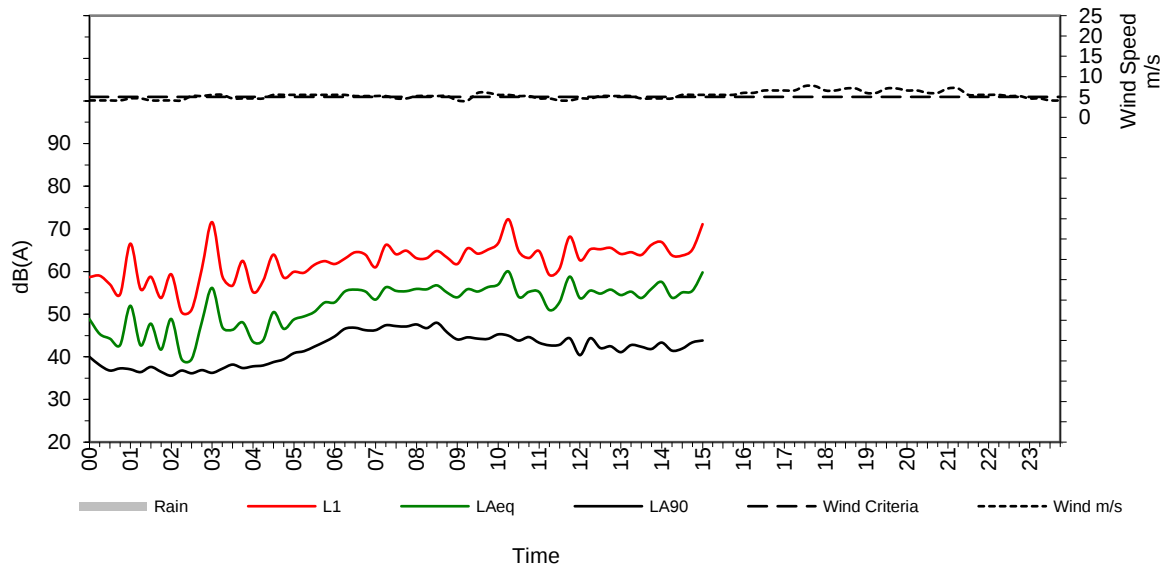
Noise Logger



Sentry 1 - Location L2

Monday 24 June 2024

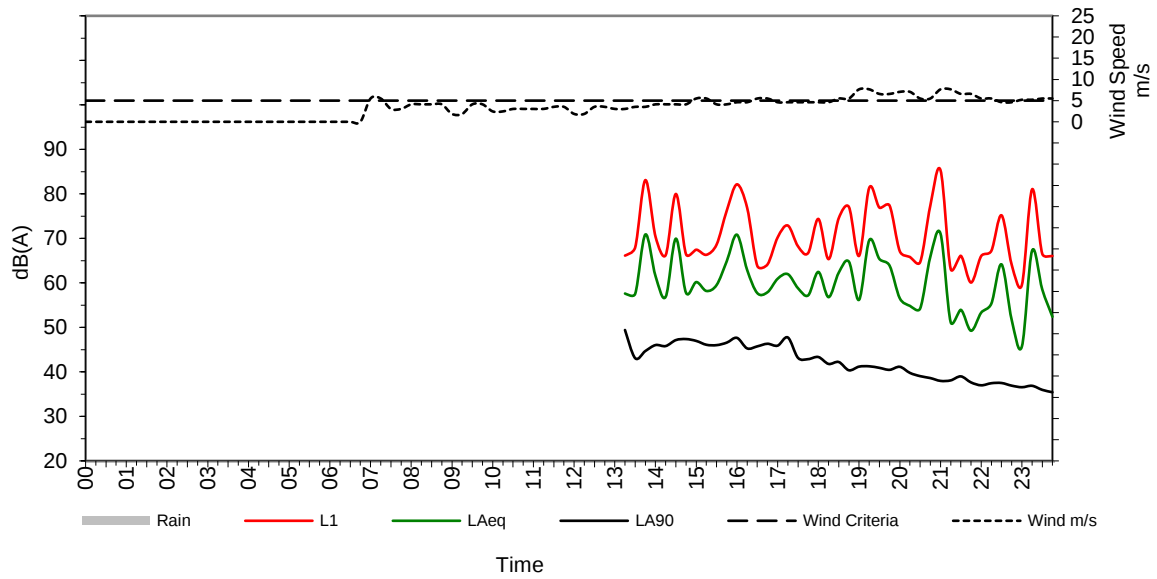
Noise Logger



Sentry 7 - Location L3

Monday 17 June 2024

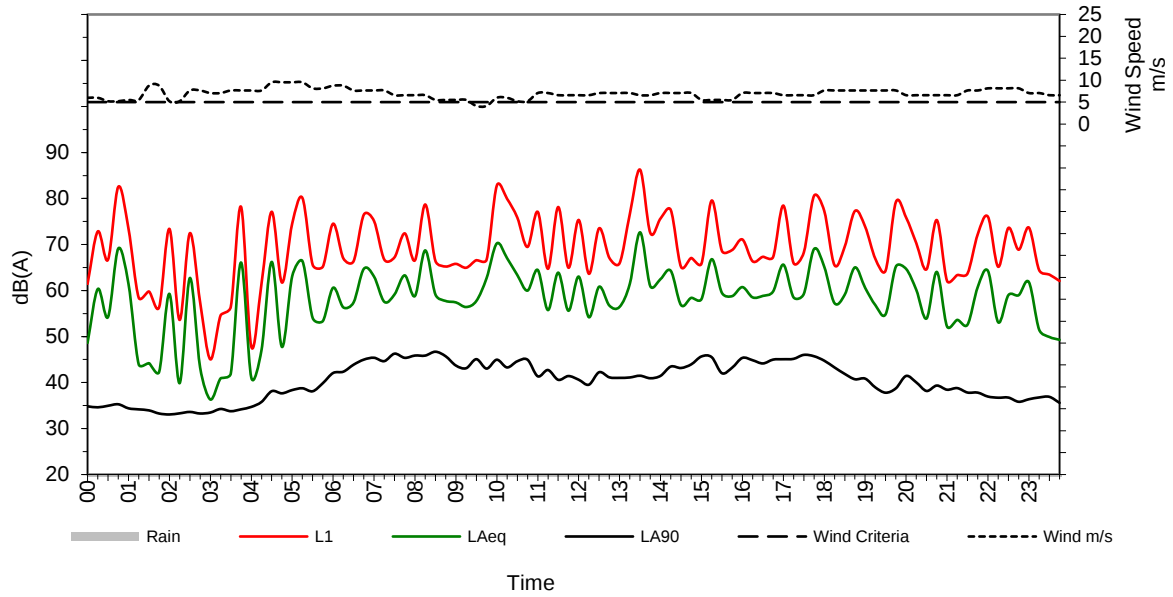
Noise Logger



Sentry 7 - Location L3

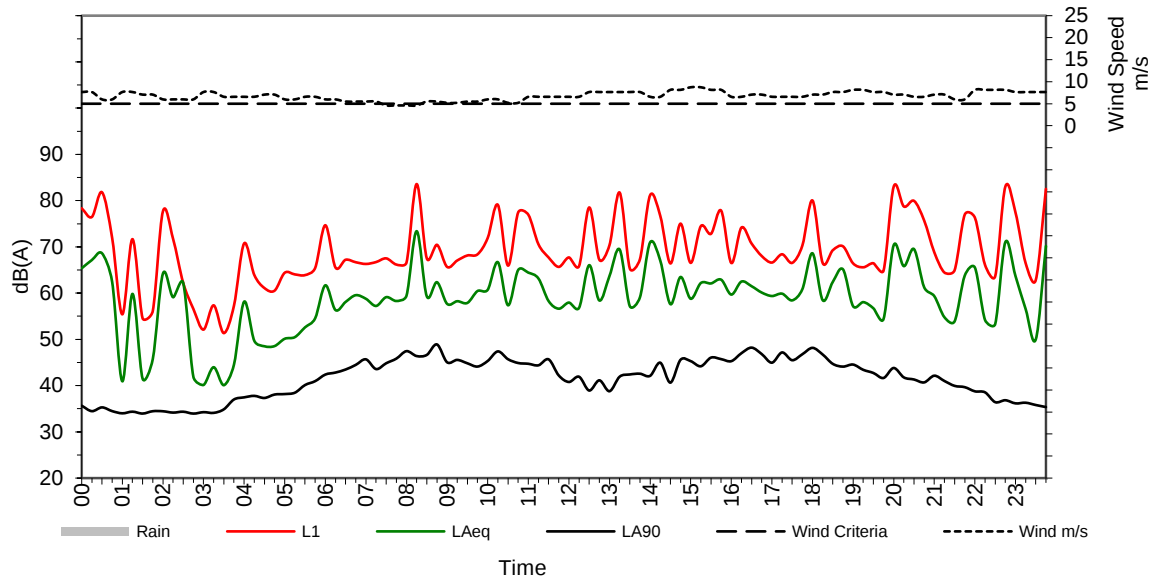
Tuesday 18 June 2024

Noise Logger



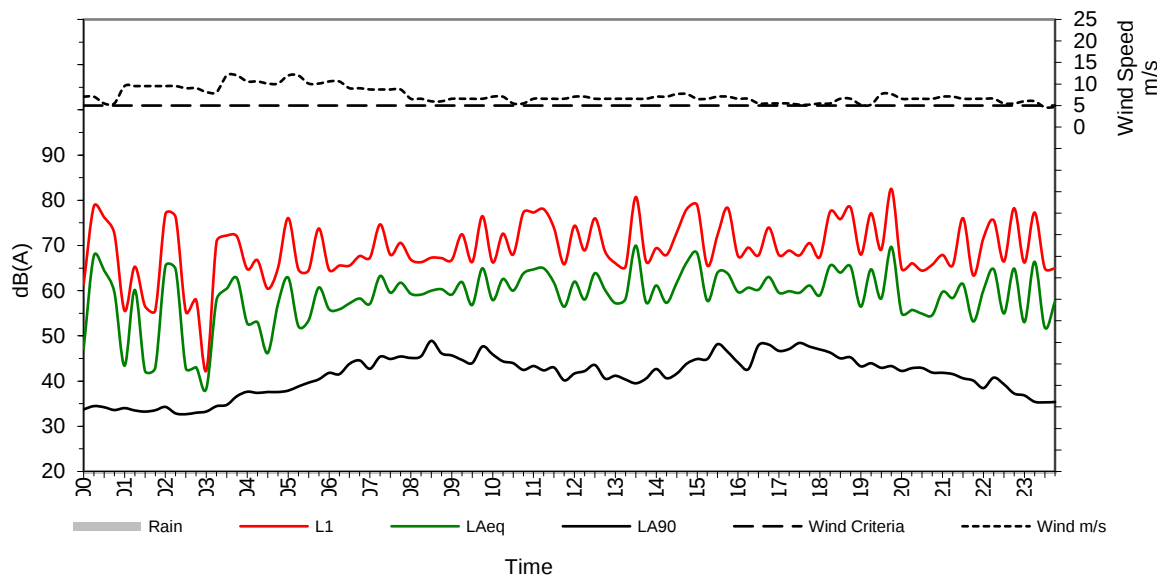
Sentry 7 - Location L3
Noise Logger

Wednesday 19 June 2024



Sentry 7 - Location L3
Noise Logger

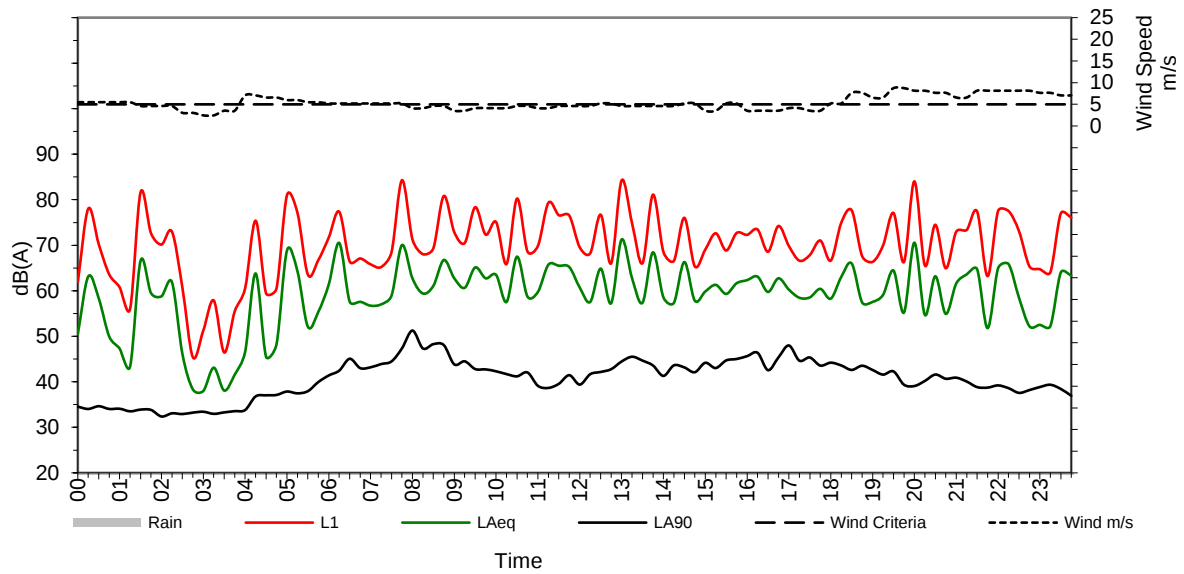
Thursday 20 June 2024



Sentry 7 - Location L3

Friday 21 June 2024

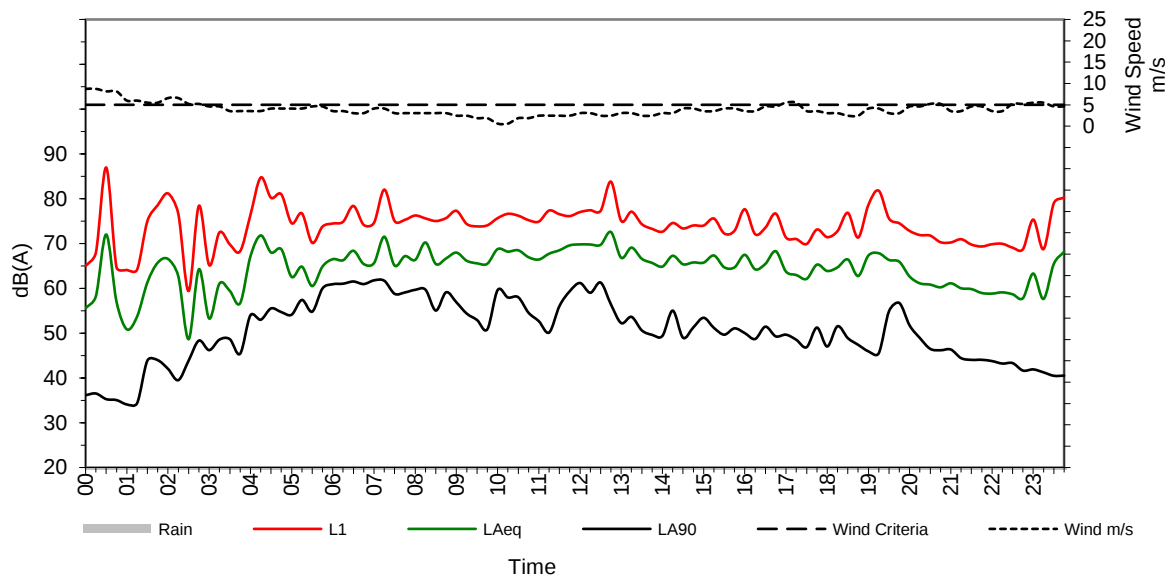
Noise Logger



Sentry 7 - Location 3

Saturday 22 June 2024

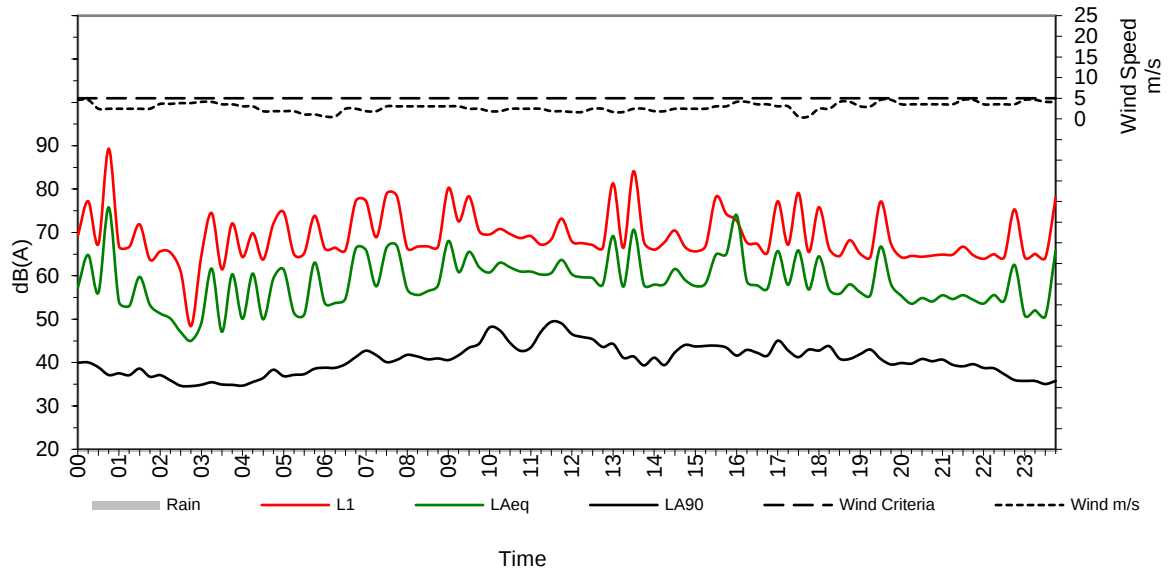
Noise Logger



Sentry 7 - Location L3

Sunday 23 June 2024

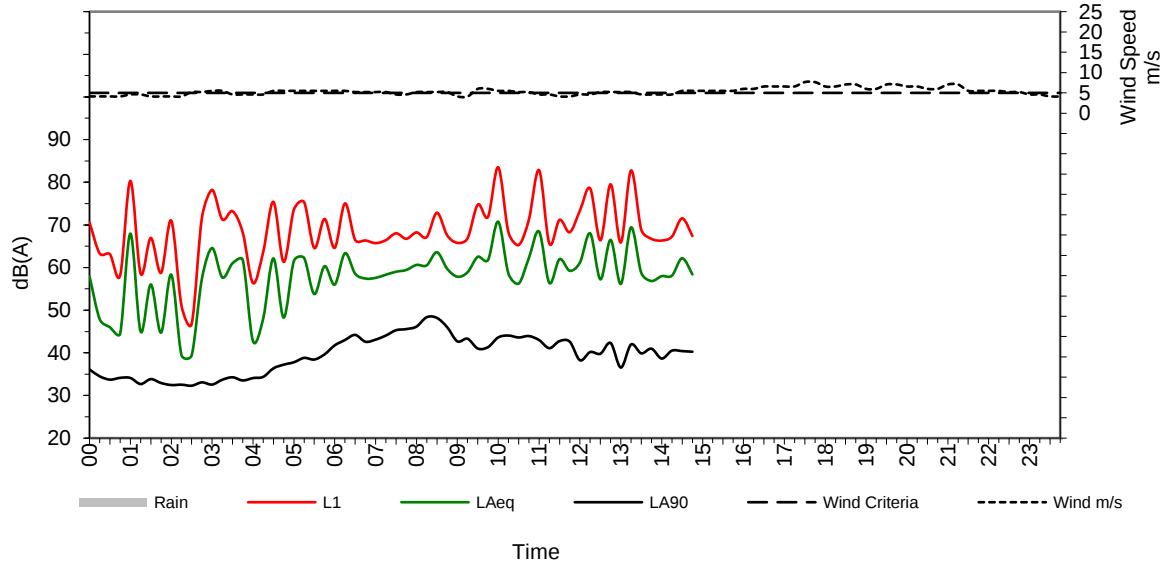
Noise Logger



Sentry 7 Location L3

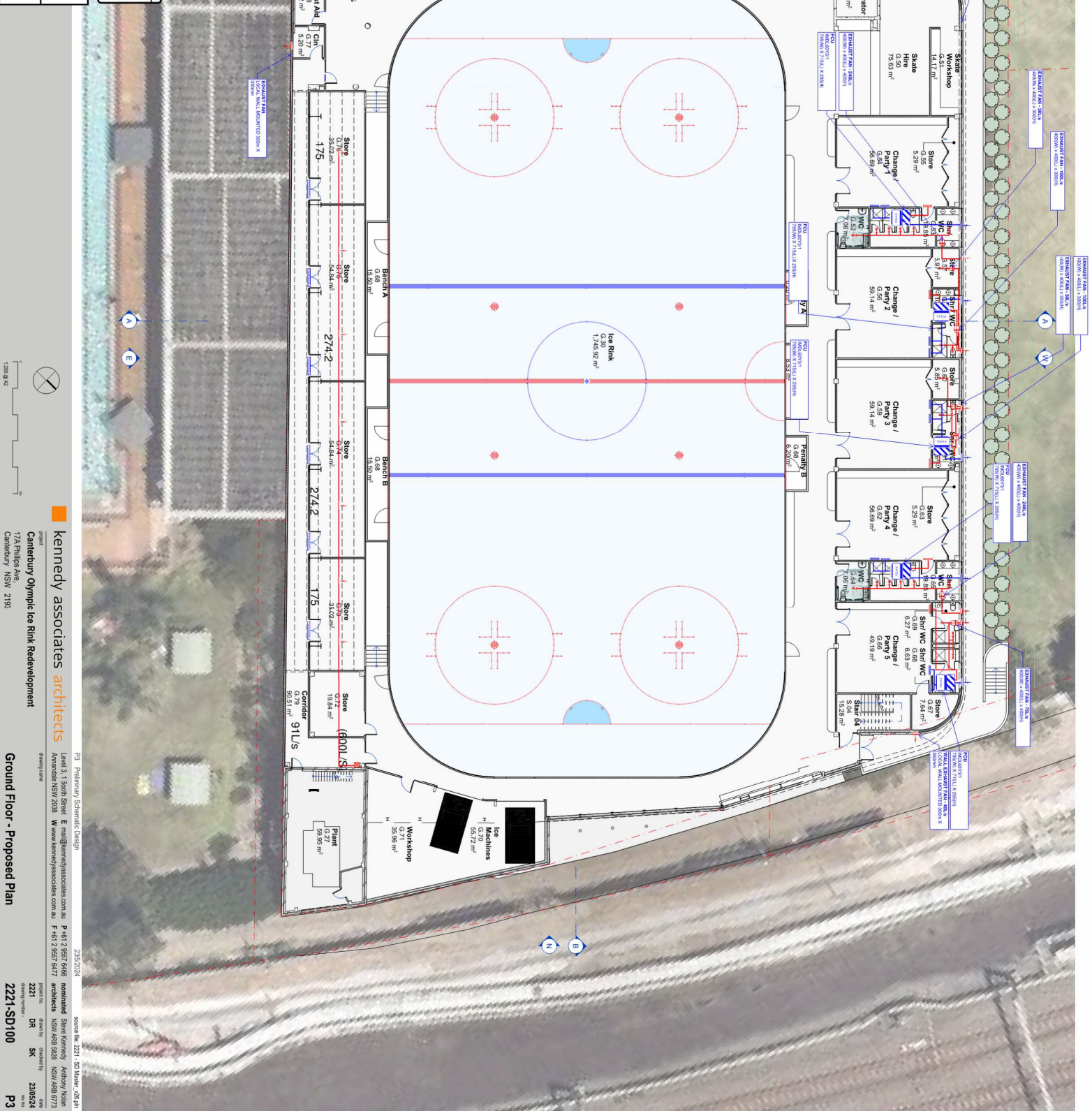
Monday 24 June 2024

Noise Logger



Appendix C

External Inlet/Outlet Locations

[illegible]

Appendix D

Plant Noise Data



Represented by:
Fantech Pty. Ltd.
 A.B.N. 11 005 434 024
 63 Vision Street
 Dandenong South VIC 3175
 Telephone: +61 (03) 9554 7845
 Facsimile: +61 (03) 9554 7833
 E-mail: info@fantech.com.au
 Version 5.7.0 Copyright © 2010-22 Elta Group

Fan: TD-1300/250 (Hi speed) Duty: 0.24 m³/s @ 250 Pa Date: 2/07/2024
 Project:
 Location: Designation:

	Octave band centre frequency,HZ							
	63	125	250	500	1K	2K	4K	8K
Sound Power Level (Inlet)	63	68	73	70	75	74	67	60
Sound Power Leaving System	63	68	73	70	75	74	67	60
Direct Sound Corrections								
Direct Sound to Terminal 100 %	0	0	0	0	0	0	0	0
Distance Listener to Terminal 3 m	-21	-21	-21	-21	-21	-21	-21	-21
Directivity(Terminal Area) <= 0.01 m	9	9	9	9	9	9	9	9
Grille Position: Corner (3 surfaces)								
Direct Sound Pressure at 3m	51	56	61	58	63	62	55	48
Reverberant Sound Corrections								
Reverberant Sound to Area 0 %	-50	-50	-50	-50	-50	-50	-50	-50
Absorption Dead Room	-1	-4	-9	-13	-15	-16	-16	-16
Room Volume Small(20 -99 m³)								
Reverberant Sound Pressure in Area	12	14	14	7	10	8	1	-6
Total Sound Pressure at 3m	51	56	61	58	63	62	55	48
Required dBA 0 dBA	17	7	0	-6	-9	-10	-10	-8
Attenuation Required	34	49	61	64	72	72	65	56
Silencer Selection	0	0	0	0	0	0	0	0
Resultant Sound Pressure at 3m	51	56	61	58	63	62	55	48

Criteria Achieved	NR 65	dBa 67	PNC 66
--------------------------	--------------	---------------	---------------



Represented by:
Fantech Pty. Ltd.
 A.B.N. 11 005 434 024
 63 Vision Street
 Dandenong South VIC 3175
 Telephone: +61 (03) 9554 7845
 Facsimile: +61 (03) 9554 7833
 E-mail: info@fantech.com.au
 Version 5.7.0 Copyright © 2010-22 Elta Group

Fan: TD-1300/250 (Hi speed) Duty: 0.24 m³/s @ 250 Pa Date: 2/07/2024
 Project:
 Location: Designation:

	Octave band centre frequency,HZ							
	63	125	250	500	1K	2K	4K	8K
Sound Power Level (Inlet)	63	68	73	70	75	74	67	60
Sound Power Leaving System	63	68	73	70	75	74	67	60
Direct Sound Corrections								
Direct Sound to Terminal 100 %	0	0	0	0	0	0	0	0
Distance Listener to Terminal 3 m	-21	-21	-21	-21	-21	-21	-21	-21
Directivity(Terminal Area) <= 0.01 m	9	9	9	9	9	9	9	9
Grille Position: Corner (3 surfaces)								
Direct Sound Pressure at 3m	51	56	61	58	63	62	55	48
Reverberant Sound Corrections								
Reverberant Sound to Area 0 %	-50	-50	-50	-50	-50	-50	-50	-50
Absorption Dead Room	-1	-4	-9	-13	-15	-16	-16	-16
Room Volume Small(20 -99 m³)								
Reverberant Sound Pressure in Area	12	14	14	7	10	8	1	-6
Total Sound Pressure at 3m	51	56	61	58	63	62	55	48
Required dBA 0 dBA	17	7	0	-6	-9	-10	-10	-8
Attenuation Required	34	49	61	64	72	72	65	56
Silencer Selection	0	0	0	0	0	0	0	0
Resultant Sound Pressure at 3m	51	56	61	58	63	62	55	48

Criteria Achieved	NR 65	dBa 67	PNC 66
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All FCU's IMDL60Y 3/1 (5 No.)

IMDL 60Y 3/1

FCU-GF-Change1 G.54

FCU-GF-Change4 G.62

Temperzone Ltd.		*** Rifled Tube Only ***		21/06/2024 10:34:51	
COIL CALCULATION					
SELECTION 11:		3/8" TUBE CHILLED GLYCOL WATER			
1: ENTRY AIR DRY.B (degC):		30.3	*** CALCULATION ***		
2: ENTRY AIR WET.B (degC):		22.0	Face Area	:	0.151 sq.m
3: ENTRY CHILLED GLYCOL :		6.0	Face Velocity	:	1.876 m/s
4: LEAVING CHILLED GLYCOL:		12.0	Leaving Dry Bulb	:	17.55 degC
5: AIR FLOW (m³/s) :		0.284	Leaving Wet Bulb	:	15.94 degC
6: FIN HEIGHT 8 (mm):			Glycol Flow	:	0.265 l/s
7: FINNED LENGTH (mm):			Glycol Velocity	:	1.322 m/s
8: No. COIL ROWS :		3	Equivalent Water Vel.	:	0.384 m/s
9: FINS PER METER :			Number of Circuits	:	3
10: No. CIRCUITS :			Sensible Cooling	:	4.38 kw
11: GLYCOL % VOLUME :		40	Sensible Heat Ratio	:	0.657
			Total Cooling	:	6.67 kw
13: Re-enter all			Air Side Friction Loss:	:	45.3 pa
14: Calculate & Display			Pressure Drop	:	0.00 kpa
0: Menu			CONNECTIONS : Same Ends		

FCU-GF-Change2 G.56

FCU-GF-Change3 G.59

Temperzone Ltd.		*** Rifled Tube Only ***		21/06/2024 10:38:39	
COIL CALCULATION					
SELECTION 11:		3/8" TUBE CHILLED GLYCOL WATER			
1: ENTRY AIR DRY.B (degC):		30.3	*** CALCULATION ***		
2: ENTRY AIR WET.B (degC):		22.0	Face Area	:	0.151 sq.m
3: ENTRY CHILLED GLYCOL :		6.0	Face Velocity	:	1.955 m/s
4: LEAVING CHILLED GLYCOL:		12.0	Leaving Dry Bulb	:	17.69 degC
5: AIR FLOW (m³/s) :		0.296	Leaving Wet Bulb	:	16.03 degC
6: FIN HEIGHT 8 (mm):			Glycol Flow	:	0.273 l/s
7: FINNED LENGTH (mm):			Glycol Velocity	:	1.358 m/s
8: No. COIL ROWS :		3	Equivalent Water Vel.	:	0.397 m/s
9: FINS PER METER :			Number of Circuits	:	3
10: No. CIRCUITS :			Sensible Cooling	:	4.52 kw
11: GLYCOL % VOLUME :		40	Sensible Heat Ratio	:	0.659
			Total Cooling	:	6.85 kw
13: Re-enter all			Air Side Friction Loss:	:	48.6 pa
14: Calculate & Display			Pressure Drop	:	0.00 kpa
0: Menu			CONNECTIONS : Same Ends		

Temperzone Ltd.

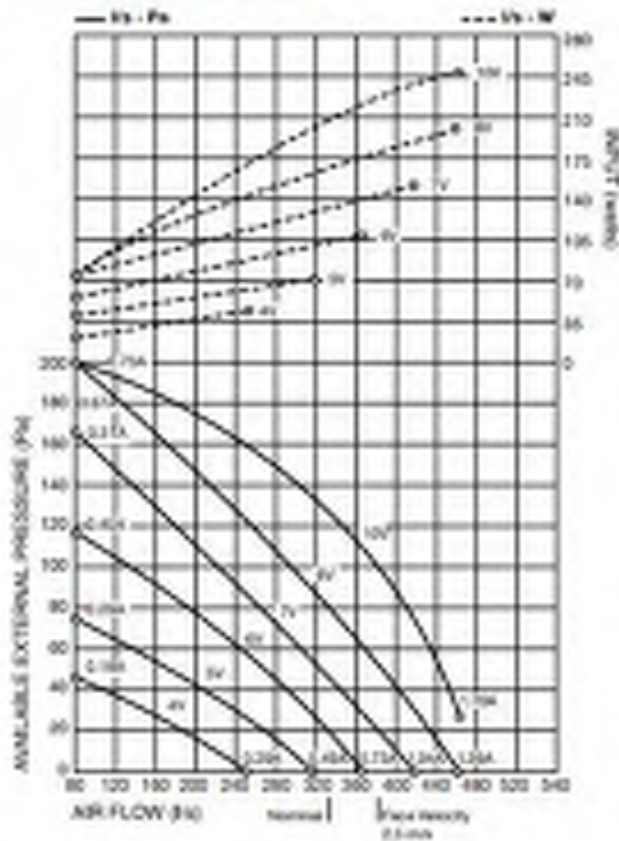
*** Rifled Tube Only ***

21/06/2024 10:40:43

CHILL CALCULATION

SELECTION 11: 2/8 TUBE CHILLED GLYCOL WATER		*** CALCULATION ***	
1: ENTRY AIR DRY.B (degC):	30.3	Face Area :	0.151 sq.m
2: ENTRY AIR WET.B (degC):	22.0	Face Velocity :	1.625 m/s
3: ENTRY CHILLED GLYCOL :	6.0	Leaving Dry Bulb :	17.05 degC
4: LEAVING CHILLED GLYCOL:	12.0	Leaving Wet Bulb :	15.61 degC
5: AIR FLOW (m ³ /s) :	0.246	Glycol Flow :	0.241 l/s
6: FIN HEIGHT 8 (mm):		Glycol Velocity :	1.202 m/s
7: FINNED LENGTH (mm):		Equivalent Water Vel. :	0.342 m/s
8: NO. COIL ROWS :	3	Number of Circuits :	3
9: FINS PER METER :		Sensible Cooling :	3.94 kw
10: NO. CIRCUITS :		Sensible Heat Ratio :	0.650
11: GLYCOL % VOLUME :	40	Total Cooling :	6.06 kw
13: Re-enter all		Air Side Friction Loss:	35.5 pa
14: Calculate & Display		Pressure Drop :	0.00 kpa
0: Menu		CONNECTIONS :	Same Ends

Air Handling



MX² 80 Plus system

Unit Submittal Data



System name	Canterbury Ice Rink June 2024
Genesys no	G364815-1
Labels	
Prepared by	Ian Air
Print date	28/06/2024 03:29:33
Program version	2024.6.19.23559+97d9925a3e3f2dd7f42344b08 f9cb2156a4a01be

System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Technical datasheet

Specification Munters dehumidifier

System



- The MX² combines traditional Munters strengths like efficiency and robustness with modern state of the art technology like modulating RH control and communication. Low energy consumption and reliability are important in todays processes. Our modern control system together with the high efficient fans with frequency converters and the Energy Recovery Purge (ERP) or Energy Efficiency Purge (EEP), ensure optimal energy savings.

Features include:

- Efficient dehumidification between -20°C and 40°C
- Modulating humidity control including wet air temp sensor
- Communication and external control options
- Filter and rotor stop alarm as standard
- Energy saving options
- Service and running indicator alarm as external indicators
- Munters Connected Climate® (MCC)
- Plenum fan for public areas

Cooling coil

- Cooling coil fitted out with an inclined stainless steel collection pan. Condensing cooler with drip-catcher and loose syphon tube.

Technical data Munters dehumidifier

General information

DH Model	MX ² 80
Controller type	Munters control system
Grid Voltage/Phase/Frequency	400/3/50
Water Removed	67.5 kg/h
Max water removed	67.5 kg/h

Process side

Air flow in	10800 Sm ³ /h
Outlet temperature	28.3 °C
Outlet moisture	2 g/kg
Air out relative pressure	299 Pa
Bag filter grade (EN 779)	Without
Panel filter grade (EN 779)	G4

Regeneration side

Air flow in	2520 Sm ³ /h
Panel filter grade (EN 779)	G4
Bag filter grade (EN 779)	Without
React heater type	Electric
Reactivation heater rated power	84.00 kW
Reactivation heater reqd. power	84.01 kW
Outlet temperature	44.4 °C
Outlet moisture	38.62 g/kg
Air out relative pressure	300 Pa

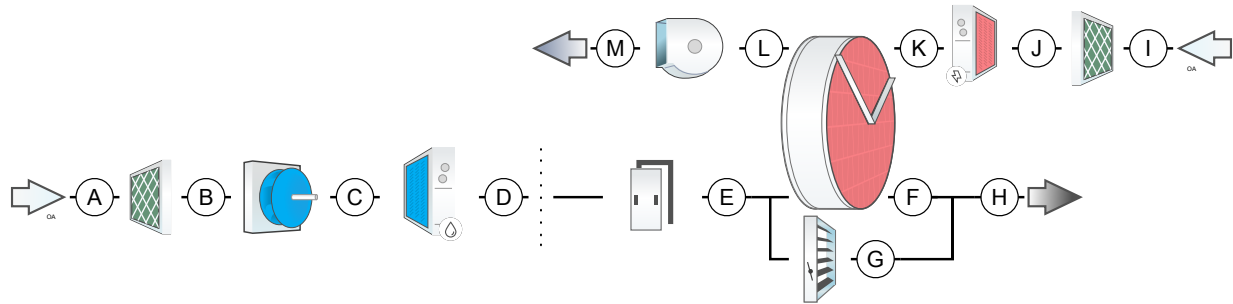
Dimension / weight / others

System total reqd. elect. power	91.73 kW
System total rated elect. power	97.72 kW
System total reqd. elect. current	136.80 A
System total rated elect. current	139.05 A
System weight	1708 kg

System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Flow diagram



Climate data location: Australia, SYDNEY CANTERBURY 3 m / 1012.9 mbar

Summer

	A	B	C	D	E	F	G	H	I	J	K	L
Sl/s	3000	3000	3000	3000	3000	2579	421	3000	700	700	700	700
°C	25.2	25.2	26.8	9.0	9.0	31.4	9.0	28.3	25.2	25.2	124.4	42.8
dp°C	21.70	21.68	21.88	8.85	8.85	-15.22	8.78	-8.41	21.70	21.68	21.68	35.70
% r.H.	81	81	74	99	99	4	98	8	81	81	1	68
Pa	0	-154	1095	818	818	329	299	299	0	-135	-160	-760

	M
Sl/s	700
°C	44.4
dp°C	35.89
% r.H.	64
Pa	300

Winter

	A	B	C	D	E	F	G	H	I	J	K	L
Sl/s	3000	3000	3000	3000	3000	2579	421	3000	700	700	700	700
°C	3.7	3.7	5.2	5.2	5.2	14.1	5.2	12.8	3.7	3.7	62.7	30.0
dp°C	-5.08	-5.10	-4.96	-4.99	-4.99	-26.11	-5.05	-19.83	-5.08	-5.10	-5.10	14.09
% r.H.	50	50	46	46	46	4	45	7	50	50	2	38
Pa	0	-151	1042	818	818	360	299	299	0	-132	-157	-658

	M
Sl/s	700
°C	31.4
dp°C	14.24
% r.H.	35
Pa	300

System capacities

Total Dehumidification 188.9 kg/h
Dehumidifier 67.5 kg/h
Cooling Coil 121.4 kg/h

Dehumidification @ maximum capacity

System utilities

System total rated power 97.7 kW
System rated current 139.1 A
Chilled Water 6.52 l/s

System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Summary

Number of systems 1
System configurations 1 x Canterbury Ice Rink June 2024 (G364815-1)

System

System arrangement	MX ² Plus
DH Model	MX ² 80
React heater type	Electric
Airflow direction	Left to right
Grid Voltage/Phase/Frequency	400/3/50
Case number	AUSTRALIA
System connection side	Back
Controller type	Munters control system
System weight	1708 kg

Operating conditions

Operating temperature, minimum	-20.0 °C
Operating temperature, maximum	40.0 °C
Installation altitude, maximum	2000 m

Transport and Storage

Minimum temperature for transport and storage	-20.0 °C
Temperature range for transport and storage, Maximum	70.0 °C
Packaging	Standard pallet

Control system

Process fan mode	On demand
------------------	-----------

Totals

Water Removed	67.46 kg/h
System total rated elect. power	98 kW
Air flow	10800 Sm ³ /h

Prepared by Ian Air
Print date 28/06/2024
Labels

Assembly

Panel filter

Design

Options

Pressure indicator quantity	1
-----------------------------	---

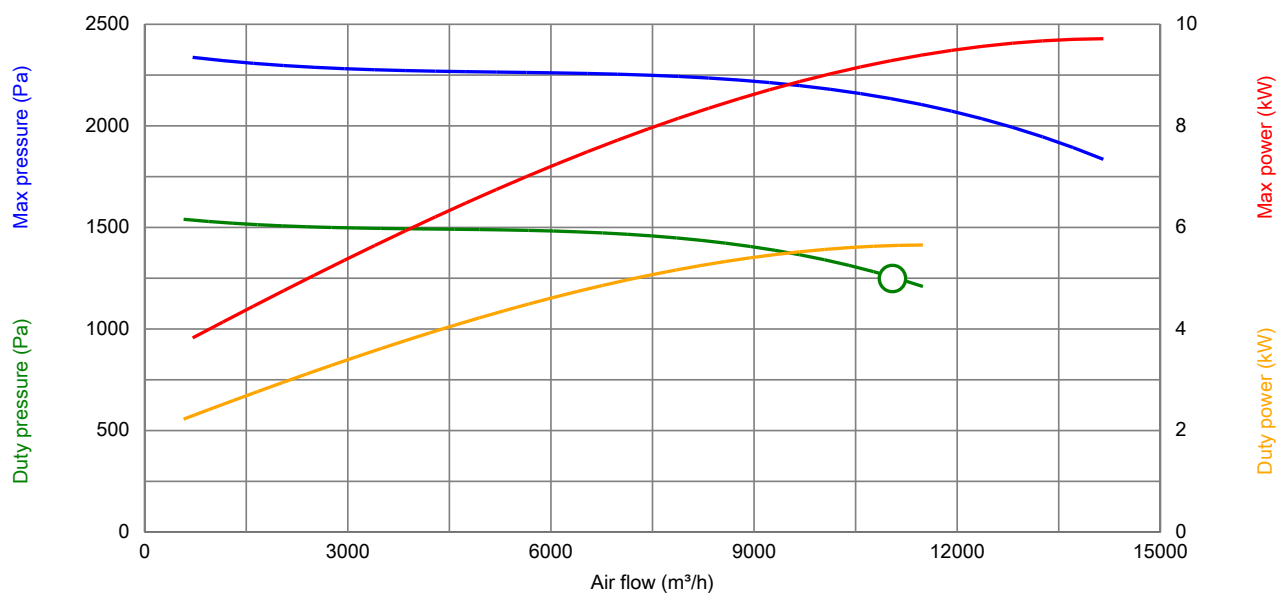
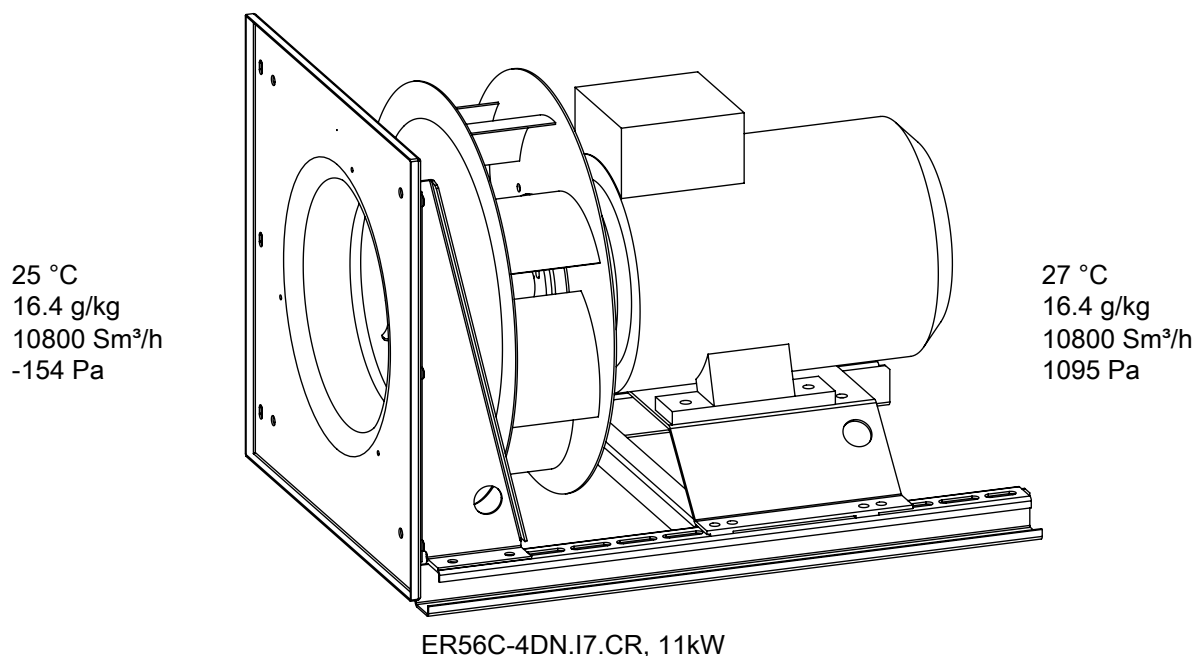
Panel filter

Panel filter pressure drop dirty	250 Pa
----------------------------------	--------

System Type MX² 80 Plus system
 Size 1818
 Genesys no G364815-1
 Name Canterbury Ice Rink June 2024

Prepared by Ian Air
 Print date 28/06/2024
 Labels

Technical data - Supply fan, pushing



System Type MX² 80 Plus system
 Size 1818
 Genesys no G364815-1
 Name Canterbury Ice Rink June 2024

Prepared by Ian Air
 Print date 28/06/2024
 Labels

Main selections

Door Left hinged
 Pressure indicator PRESSURE, DIFF TRANSM. 0-7000
 Inspection side Right
 Fan Model ER56C-4DN.I7.CR, 11kW
 Frequency control Yes

Results

Component total rated electric current 12.3 A
 Component total rated electric power 11.0 kW

Sound

	63	125	250	500	1k	2k	4k	8k	dB(A)
Sound power levels at suction side	71.2	70.7	82.7	72.3	74.8	74.4	71.3	69.4	80.8
Sound power levels at pressure side	80.3	78.2	86.0	83.3	83.9	79.9	76.2	72.1	87.7

1 x

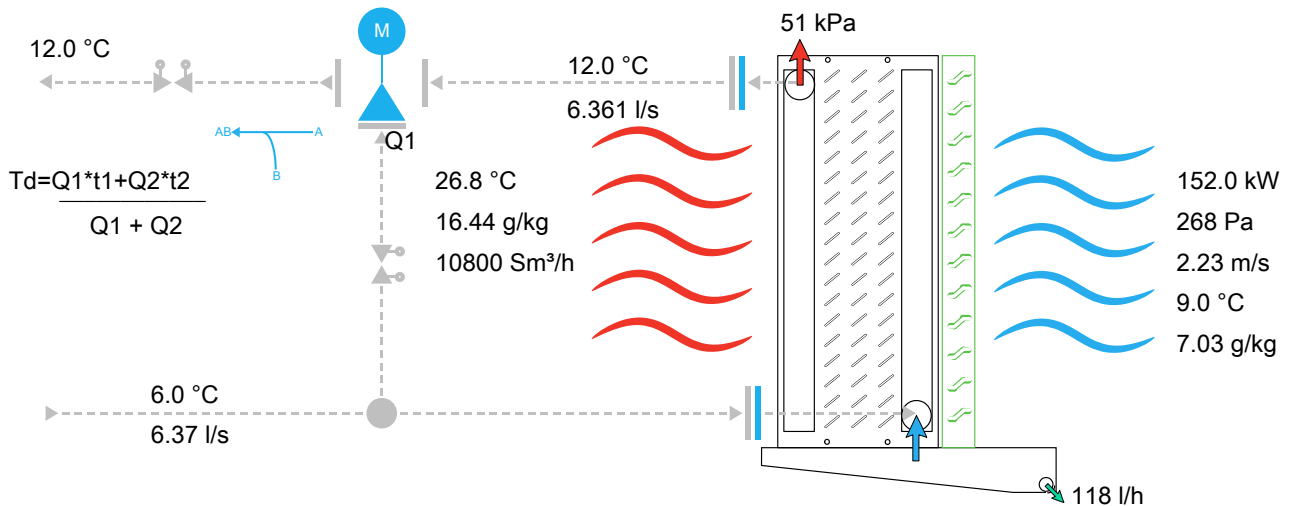
Main selections

Frequency inverter INVERTER,FREQUENCY,FC101 IP54 15KW

System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Technical data - Precooler, ethylene glycol



Design

Fluid temperature in 6.0 °C
Fluid temperature out 12.0 °C

Coil casing

Connection side Left
Coil frame material FeZn 2.0 mm
Coil dimensions 1335x1290
Cooling coil fluid drainage Sloped tray, Inox 304

Tubes

Tube material Copper
Tube diameter 9.9 mm (3/8")
Tube thickness 0.30 mm
Number of tube rows 12
Number of circuits 72

Fins

Fin material Aluminium
Fin thickness 0.2 mm
Fin spacing 2 mm

Fluid

Fluid Ethylene glycol
Fluid antifreeze by weight 20.00 %
Coil fluid inlet connection size 2 x DN 80
Fluid volume 64 L

Accessories

Coil Flanges Threaded flanges PN16
Frost Protection None
Droplet eliminator Removable polypropylene HT 33mm pitch
Mist eliminator frame Separate frame, FeZn

Coil Data

PED design pressure (barg) 15 bar
PED CAT. Art. 4 Par. 3 seen as Piping
PED Class Art 4.3

1 x Valve, precooler, ethylene glycol

Coil

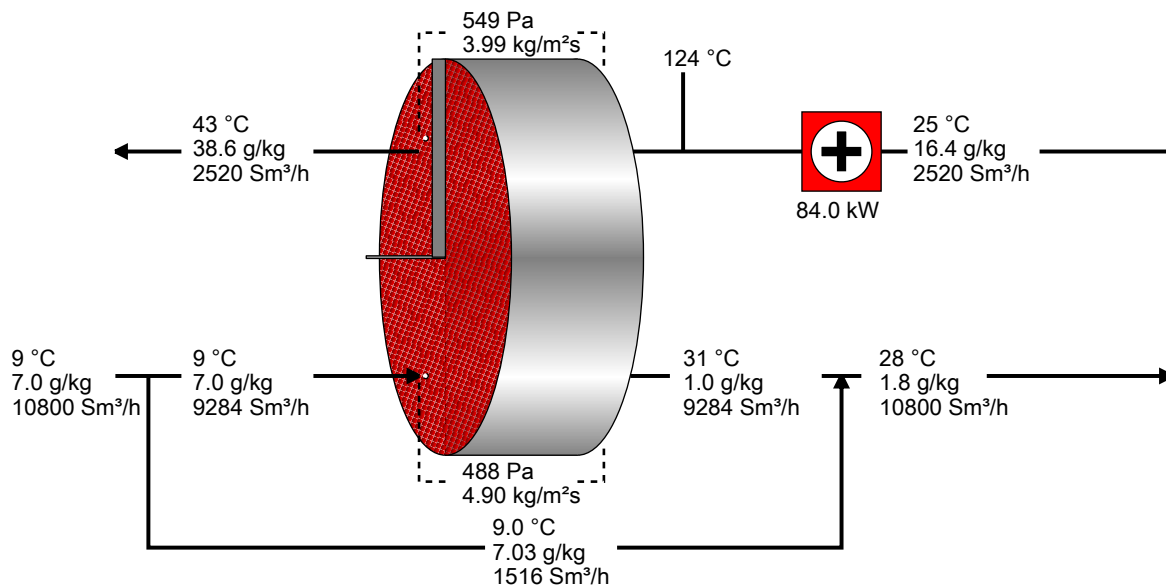
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Labels

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System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Technical data - Dehumidifier



Main selections

DH Model
Desiccant rotor type
Material
Grid Voltage/Phase/Frequency
Airflow direction
Insulated process inlet
Purge
DH Bypass

Weight

Estimated weight

Options

Humidity transmitter
User Manual

React Heater

Reactivation heater reqd. power
Reactivation heater max. power
Air flow out

Outlet temperature
Outlet moisture

Process

Outlet temperature
Outlet moisture

React

Air flow out
Outlet temperature
Outlet moisture
Air pressure drop

Drive motor

Drive motor rated power

Rotor

Air flow out

MX²80
HPS
Aluzink
400/3/50
Left to right
Yes
None
Yes, internal

564 kg

RH+T (Duct mounted)
GB

84.0 kW
102.0 kW
2520 Sm³/h
124 °C
16.4 g/kg

28 °C
1.8 g/kg

2520 Sm³/h
43 °C
38.6 g/kg
624 Pa

0.02 kW

9284 Sm³/h

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Outlet temperature	31 °C
Outlet moisture	1.0 g/kg
Air pressure drop	488 Pa
Bypass	
Outlet temperature	9.0 °C
Outlet moisture	7.03 g/kg
Dehumidifier	
Component total electric power	84.0 kW
Component total rated electric power	84.02 kW
Component total electric current	121.37 A
Component total rated electric current	121.37 A

System Type MX² 80 Plus system
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Technical data - Filter bank, React

Panel filter

Panel filter grade (EN 779)	G4
Panel filter quantity	1
Panel filter size 1	592x392x95
Panel filter part no.1	190112300-7 (1pcs)

Options

Pressure indicator	Pressure Switch 50-500Pa QBM9903-5
Pressure indicator quantity	1

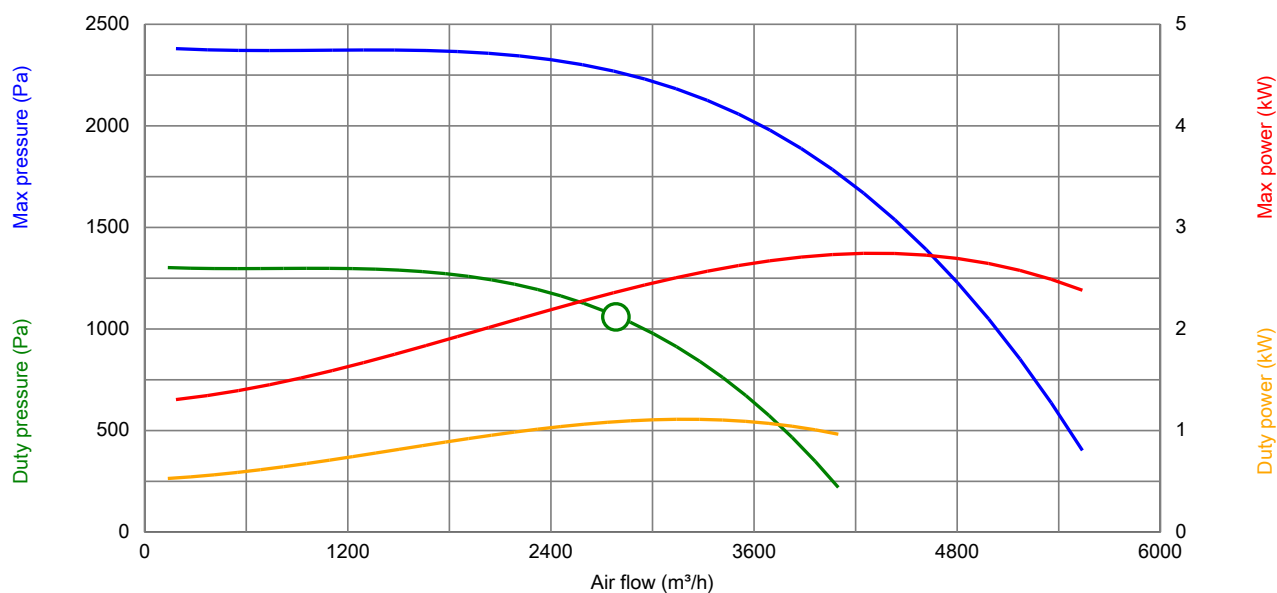
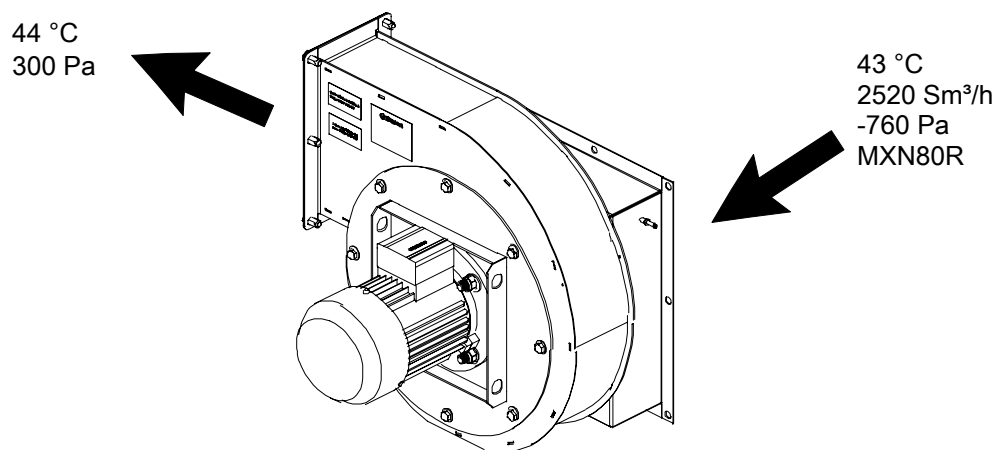
Filter

Filter pressure drop design	135 Pa
Filter pressure drop dirty	200 Pa
Face velocity	3.10 m/s

System Type MX² 80 Plus system
 Size 1818
 Genesys no G364815-1
 Name Canterbury Ice Rink June 2024

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Technical data - Reactivation fan



System Type	MX ² 80 Plus system
Size	1818
Genesys no	G364815-1
Name	Canterbury Ice Rink June 2024

Prepared by	Ian Air
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Main selections

DH Model	MX ² 80
React fan outlet	Back
Frequency control, react	Yes
Fan outlet connection size	502x291 (450x231)

Frequency

Fan set point frequency	50Hz
-------------------------	------

Results

Fan speed	2641 rpm
Fan pressure rise	1060 Pa
Component total rated electric current	4.66 A
Component total rated electric power	2.20 kW

System Type MX² 80 Plus system
 Size 1818
 Genesys no G364815-1
 Name Canterbury Ice Rink June 2024

Prepared by Ian Air
 Print date 28/06/2024
 Labels

Technical data - Control system

Control system

Controller type	Munters control system
HMI	Text display
Communications protocols	No
Munters Connected Climate®	No

Humidity control

Humidity transmitter	RH+T (Duct mounted)
Sensor control	Relative Humidity
Sensor 2	None
Sensor 3	No
Sensor 4	No
Temperature sensor	None
Frost protection pre react heater	None
Temperature sensor	None

Options

External humidity control	No
External temperature setpoint	No
CO2 Sensor	No
CO2 damper output	No
Floating dew point control	No
Re-transmission control	No
Re-transmission signal	No
Re-transmission control nr.2	No
Re-transmission signal nr.2	No

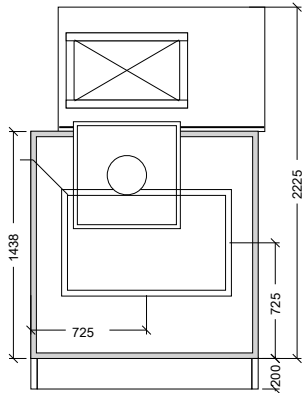
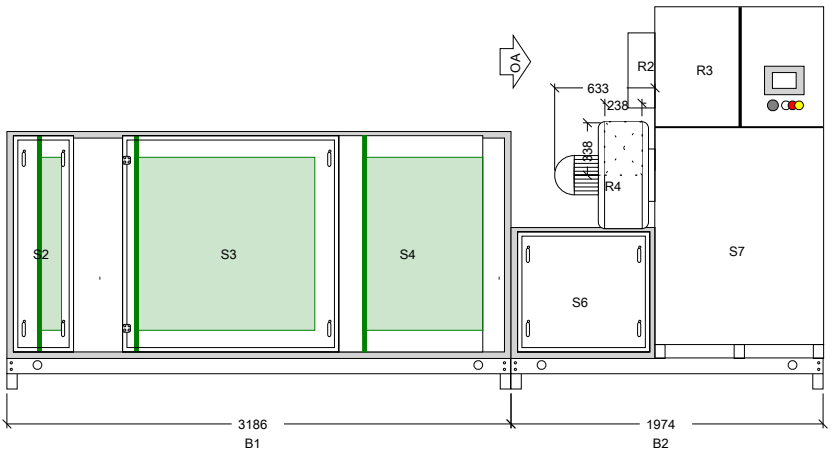
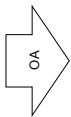
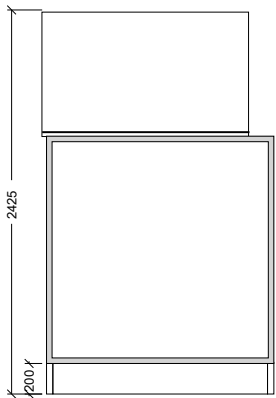
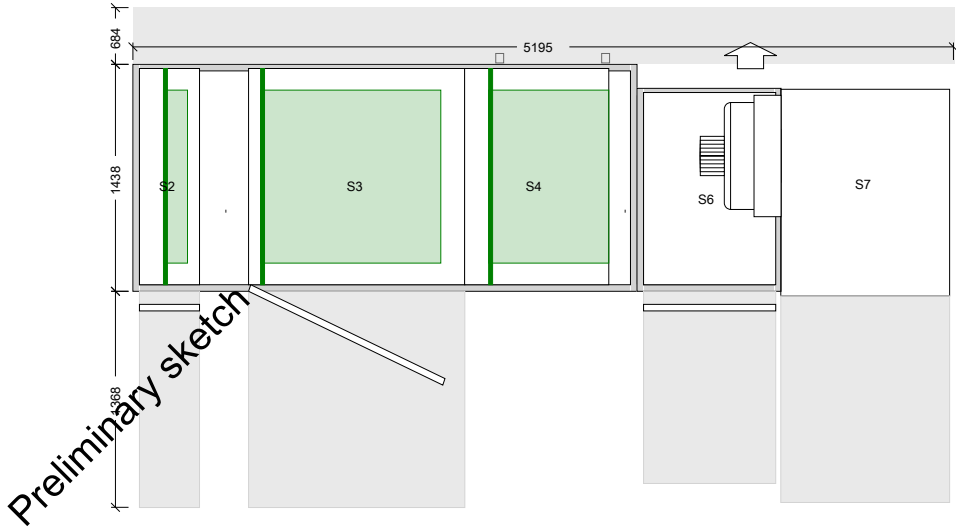
System

Process pretreatment temp sensor	PT1000
Limitation temp sensor	None
Pre reactactivation heater control	None

System Type	MX ² 80 Plus system
Size	1818
Genesys no	G364815-1
Name	Canterbury Ice Rink June 2024

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Labels	

Technical data - Spare parts



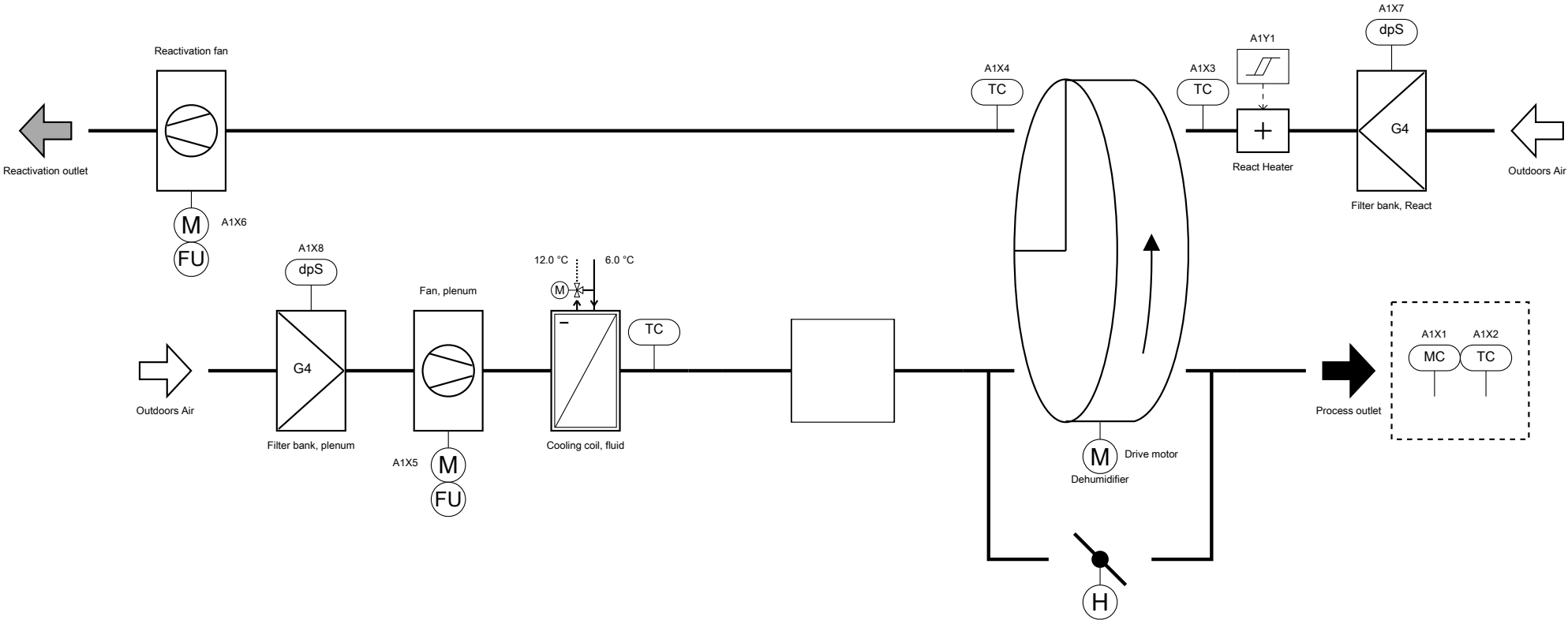
- S1 - Process inlet
- S2 - Pretreatment filter
- S3 - Supply fan, pushing
- S4 - Precooler, ethylene glycol
- S5 - Box split
- S6 - Section, Empty/Access
- S7 - Dehumidifier
- S8 - Process outlet

- R1 - Reactivation inlet
- R2 - Filter bank, React
- R3 - Dehumidifier
- R4 - Reactivation fan
- R5 - Reactivation outlet

System weight 1708 kg

System name Canterbury Ice Rink June 2024		
Tolerances, if not indicated, according to 160-010266-001		
Design by Ian Air		Genesys no G364815-1

Preliminary sketch (not to scale)



System	
System arrangement	MX² Plus
Pre/post treatment	Pre
Process pretreatment temp sensor	PT1000
Limitation temp sensor	None
Frost protection pre react heater	None
Precooler	Yes
Post-treatment is present	No
Humidifier present	No
Post cooler or heater present	no
Unit	Humidity sensor
	Humidity transmitter
Control system	Humidity sensor
	Humidity transmitter
Controller type	Humidity sensor
	Humidity transmitter
HMI	Humidity sensor
	Humidity transmitter
Communications protocols	Humidity sensor
	Humidity transmitter

Yes	System name
No	Canterbury Ice Rink June 2024
No	Tolerances, if not indicated, according to
No	160-010266-001
No	P&ID
No	Genesys no
No	G364815-1
No	Design by
No	Ian Air

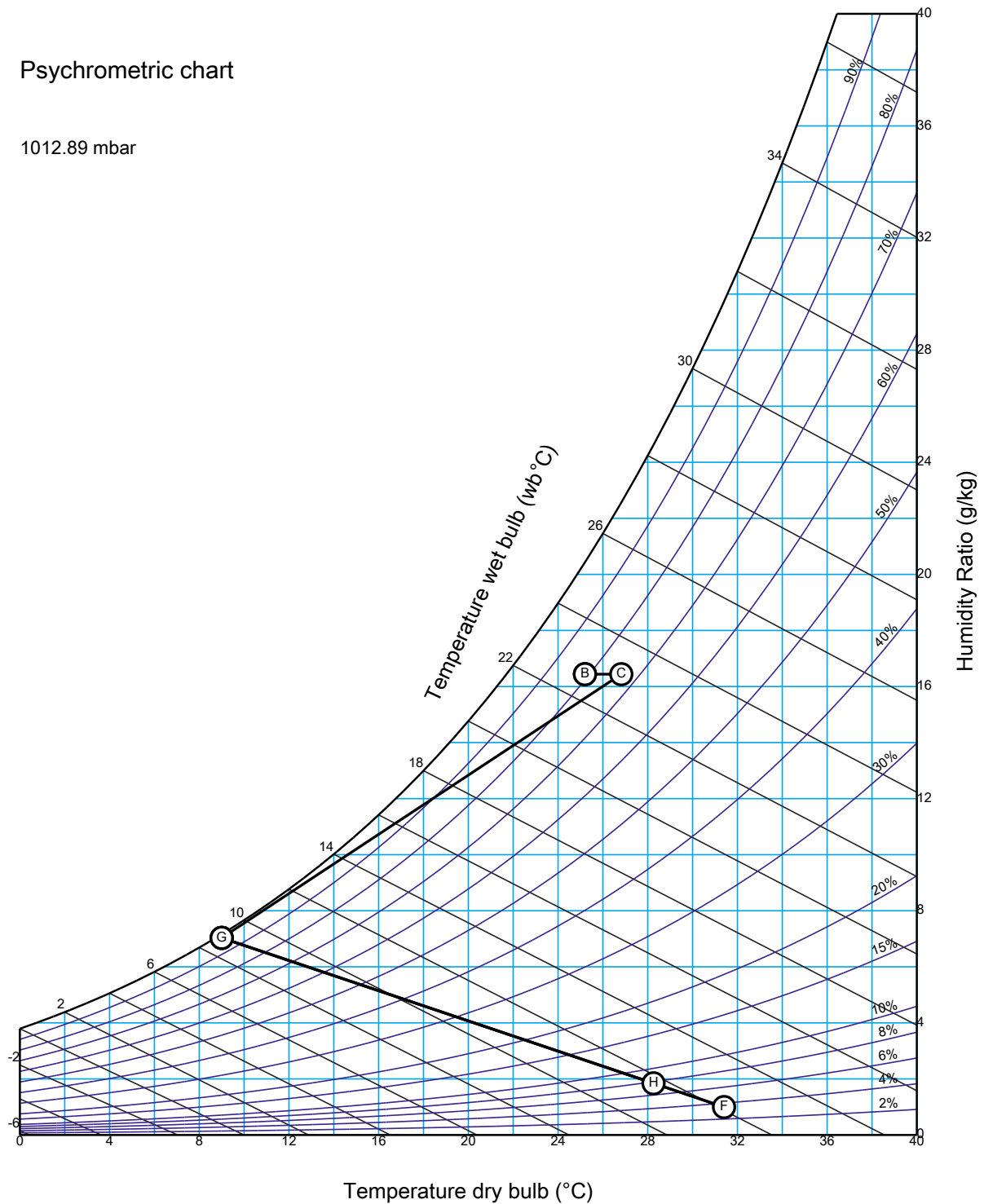
System Type MX² 80 Plus system
Size 1818
Genesys no G364815-1
Name Canterbury Ice Rink June 2024

Prepared by
Print date 28/06/2024
Labels

Psychrometric chart - Summer

Psychrometric chart

1012.89 mbar



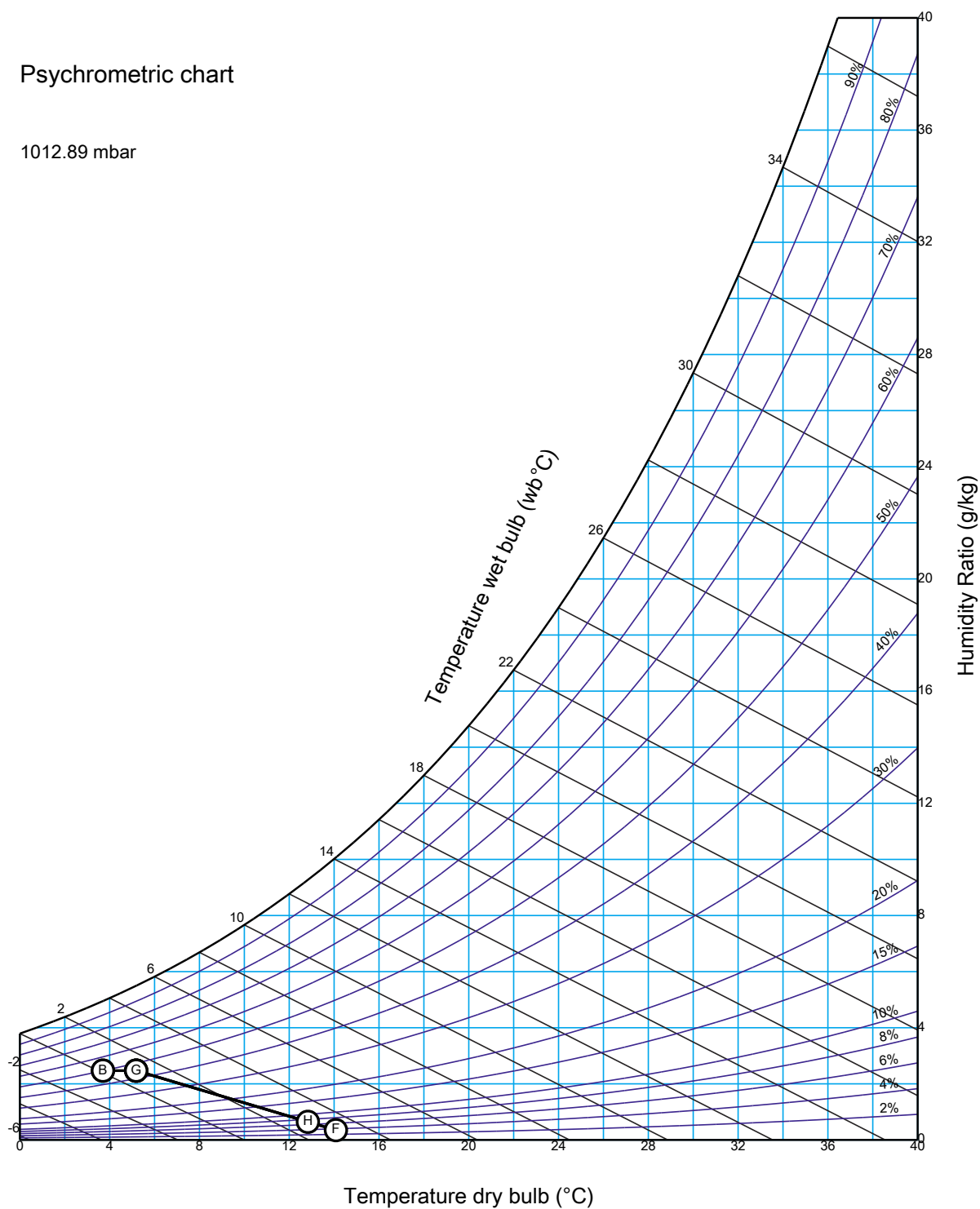
System Type MX² 80 Plus system
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Name Canterbury Ice Rink June 2024

Prepared by Ian Air
Print date 28/06/2024
Labels

Psychrometric chart - Winter

Psychrometric chart

1012.89 mbar





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Fan: TD-1300/250 (Hi speed) Duty: 0.24 m³/s @ 250 Pa Date: 2/07/2024
 Project:
 Location: Designation:

	Octave band centre frequency,HZ							
	63	125	250	500	1K	2K	4K	8K
Sound Power Level (Inlet)	63	68	73	70	75	74	67	60
Sound Power Leaving System	63	68	73	70	75	74	67	60
Direct Sound Corrections								
Direct Sound to Terminal 100 %	0	0	0	0	0	0	0	0
Distance Listener to Terminal 3 m	-21	-21	-21	-21	-21	-21	-21	-21
Directivity(Terminal Area) <= 0.01 m	9	9	9	9	9	9	9	9
Grille Position: Corner (3 surfaces)								
Direct Sound Pressure at 3m	51	56	61	58	63	62	55	48
Reverberant Sound Corrections								
Reverberant Sound to Area 0 %	-50	-50	-50	-50	-50	-50	-50	-50
Absorption Dead Room	-1	-4	-9	-13	-15	-16	-16	-16
Room Volume Small(20 -99 m³)								
Reverberant Sound Pressure in Area	12	14	14	7	10	8	1	-6
Total Sound Pressure at 3m	51	56	61	58	63	62	55	48
Required dBA 0 dBA	17	7	0	-6	-9	-10	-10	-8
Attenuation Required	34	49	61	64	72	72	65	56
Silencer Selection	0	0	0	0	0	0	0	0
Resultant Sound Pressure at 3m	51	56	61	58	63	62	55	48

Criteria Achieved	NR 65	dBa 67	PNC 66
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Criteria Achieved	NR 65	dBa 67	PNC 66
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